# 2-GHz Single Balanced Mixer

### **Description**

The U2796B-FP is a 2-GHz down conversion mixer for telecommunication systems, e.g. cellular radio, CT1, CT2, DECT, PCN, using TELEFUNKEN advanced bipolar technology. The U2796B is well suited for the receiver

portion of the RF circuit. Single balanced structure has been chosen for the best noise performance and low current consumption. The IIP3 is programmable.

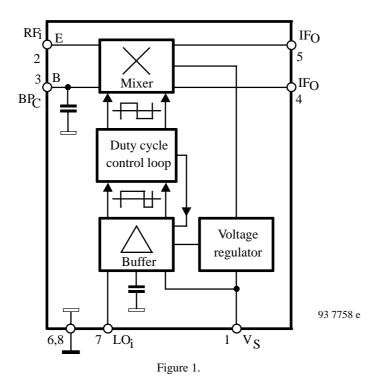
#### **Features**

- Supply voltage range: 2.7 to 5.5 V
- Exellent isolation characteristics
- Low current consumption: 3.2 mA without R<sub>IP3</sub>
- IIP3 programmable
- Input frequency operating range up to 2 GHz
- RF characteristic nearly independent of supply voltage

#### **Benefits**

- Stand alone product
- Low current consumption extends talk time
- 3-V operation requires small space for batteries

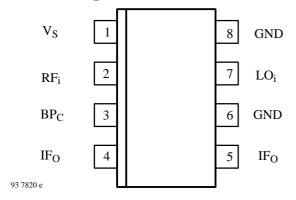
## **Block Diagram**



# **U2796B-FP**

**TELEFUNKEN Semiconductors** 

# **Pin Description**



Pin	Symbol	Function
1	$V_{S}$	Supply voltage
2	RF	RF input and IIP3 programming
		port
3	$BP_{C}$	By-pass capacitor
4	IFo	IF output
5	IFo	IF output
6	GND	Ground
7	LOi	Local oscillator input
8	GND	Ground

Figure 2.

# **Absolute Maximum Ratings**

Parameters	Symbol	Value	Unit
Supply voltage Pin 1	V <sub>S</sub>	6	V
Input voltage Pins 2, 3, 4, 5 and 7	Vi	0 to V <sub>S</sub>	V
Junction temperature	T <sub>i</sub>	125	°C
Storage temperature	T <sub>sto</sub>	-40  to + 125	°C

# **Operating Range**

Parameters	Symbol	Value	Unit
Supply voltage range Pin 1	V <sub>S</sub>	2.7 to 5.5	V
Ambient temperature	T <sub>amb</sub>	-40  to + 85	°C

# **Thermal Resistance**

Parameters	Symbol	Value	Unit
Junction ambient SO 8	$R_{thJA}$	175	K/W

## **Electrical Characteristics**

Test conditions (unless otherwise specified):

 $V_S = 3$  V,  $f_{LO} = 900$  MHz;  $I_M = 1.2$  mA,  $T_{amb} = 25$ °C. System impedance  $Z_O = 50$   $\Omega$ 

Parameters	Test conditions / Pin	Symbol	Min.	Тур.	Max.	Unit
Supply voltage	Pin 1	$V_{S}$	2.7		5.5	V
Supply current	$R_{IP3} = \infty$ , Pin 1	$I_S$	2.8	3.2	3.7	mA
Conversion power gain	$RL = 3 \text{ k}\Omega$ , $R_{IP3} = \infty$ $f_{LO} = 900 \text{ MHz}$	PG <sub>C</sub>		9		dB
Figure 4	$f_{LO} = 1700 \text{ MHz}$ $f_{IF} = 45 \text{ MHz}$			9		
Isolation	•	'		'		'
LO-spurious at RF <sub>in</sub>	$\begin{array}{c c} Pi_{LO} = -10 \text{ dBm} \\ Figure 5 & Pin 7 \text{ to } 2 \end{array}$	IS <sub>LORF</sub>			-35	dBm
RF to LO	$Pi_{RF} = -25 \text{ dBm}$ Pin 2 to 7 $f_{LO} = 900 \text{ MHz}$	IS <sub>RFLO</sub>	30	40		dB
Figure 6	$f_{LO} = 1700 \text{ MHz}$			20		
<b>Operating frequencies</b>						
RF frequency	Pin 2	RFi	2000			MHz
LO <sub>in</sub> frequency	Pin 7	LOi	2000			MHz
IF <sub>out</sub> frequency	Pins 4 and 5	IFo	300			MHz
Input level						
RF input (–1 dB comp.)	$RL = 50 \Omega$ , Pin 2	Pi <sub>RF</sub>		-15		dBm
3rd order intercept point	$Pi_{LO} = -10 \text{ dBm}, R_{IP3} = \infty$ Figure 2 Pin 2	IIP3		-4		dBm
LO input	Pin 7	$P_{iLO}$		-6	0	dBm
Impedances						
RF input	Pin 2	ZiRF		25		Ω
LO input	Pin 7	Zi <sub>LO</sub>		50		Ω
IF output	Pins 4 and 5	Z <sub>oIF</sub>		$> 10 \text{ k}\Omega//$ 0.9 pF		
Noise figure (DSB)	$Pi_{LO} = 0dBm$ , $RL > 3 kΩ$ $f_{LO} = 900 MHz$	NF <sub>50</sub>		9		dB
Figure 7	$f_{LO} = 1700 \text{ MHz}$			12		]
Voltage standing wave ratio LO	Pin 7	VSWR- LO		1.3	2	
Note: I <sub>M</sub> = Internal mixer of	urrent (see figure 2)	LU	1			

Note:  $I_M$  = Internal mixer current (see figure 2)

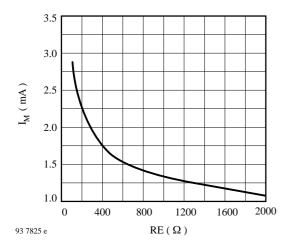


Figure 3. Mixer current  $(I_M)$  versus RE

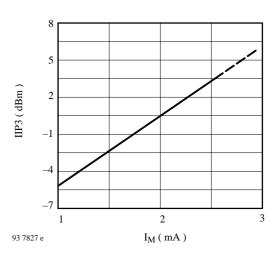


Figure 4. Third-order input intercept IIP3 point versus  $I_{M}$ 

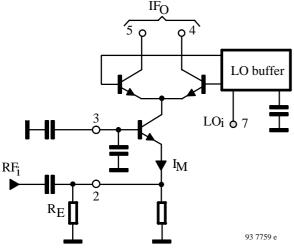


Figure 5. Mixer circuitry

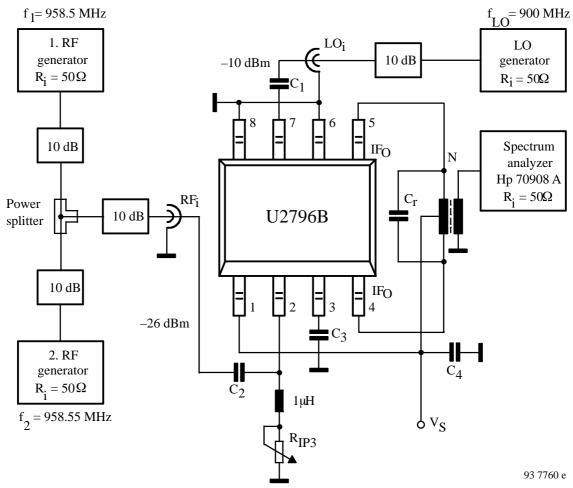


Figure 6. Test circuit-conversion power gain (PG<sub>C</sub>) and 3rd order input intercept point (IIP3)

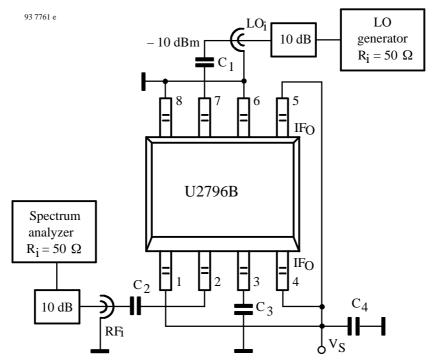


Figure 7. Test circuit-isolation LO to RF

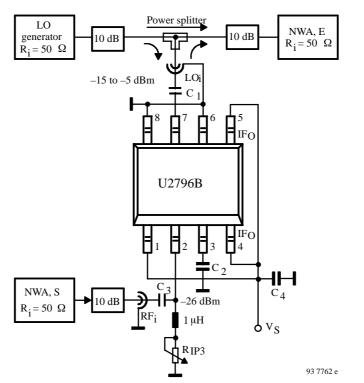


Figure 8. Test circuit-isolation RF to LO

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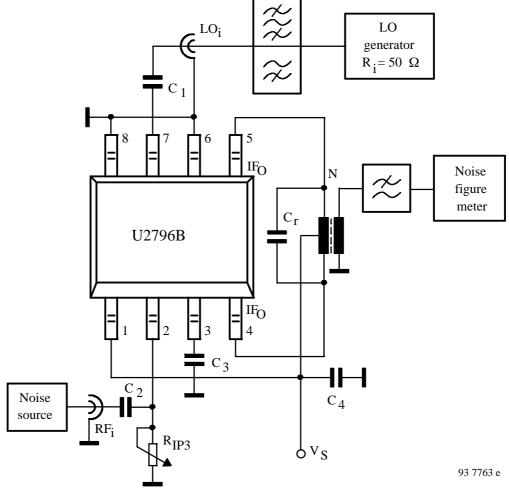


Figure 9. Test circuit-noise figure

#### Note:

- 1. The noise floor of the LO generator might influence the noise figure test result. In order to avoid this, either a band pass or a high pass filter with  $fc > f_{IF}$  should be implemented.
- 2. If IF output network does not provide sufficient suppression of the LO component, a low pass filter should be inserted to avoid overdriving the noise figure meter.
- 3. For best noise performance 0 dBm LO power level is required.

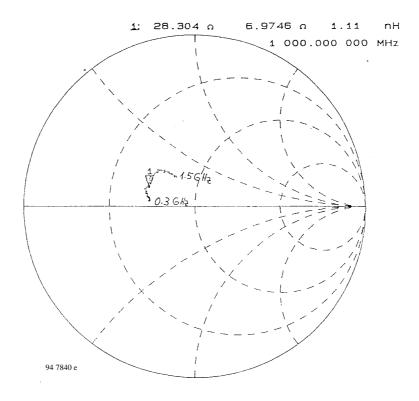


Figure 10. S11 RF input impedance

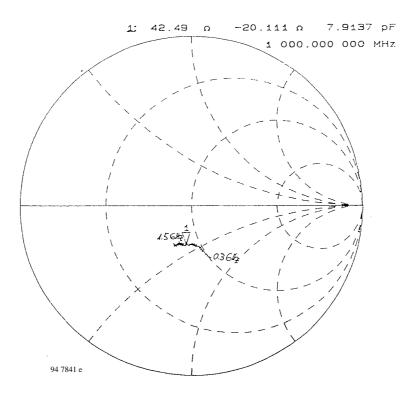


Figure 11. S11 LO input impedance

## **Application Circuit**

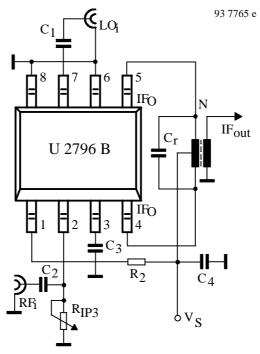


Figure 12.

#### **Recommended Values for the Evaluator**

 $C_1$  and  $C_2$  = 150 pF,  $C_3$  and  $C_4$  = 100 nF.  $C_r$  is calculated for resonance with the balun at  $f_{IF}$ , or as a high pass filter for  $f_{LO}$ . The output balun transformer ratio > = 8:1 for  $Z_O$  = 50  $\Omega$   $R_2$  increases the IF output level and is calculated from:

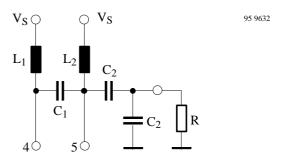
$$R_2 = \frac{V_S (4,5) - V_S (1)}{I_S (1)}$$

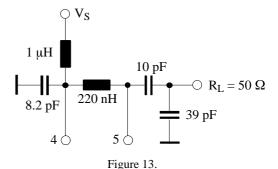
For example  $V_S$  (4,5) = 4 V,  $V_S$  (1) = 3 V,  $I_S$  (1) = 2.2 mA  $R_2 \approx 470 \,\Omega$  where  $I_S$  (1) is the current consumption without the mixer stage.

# **Application Hint**

The output transformer at the pins 4 and 5 can be replaced by LC-circuits like one of the following proposals, which are saving space compared to the transformer and are suitable for higher IF frequencies. When applying one of these solutions, it has to be checked whether the requirements on noise figure and gain can be achieved.

The second circuit was dimensioned for approximately 130 MHz and a load resistance of 50  $\Omega$ . If for instance the impedance of a subsequent filter is 1 k $\Omega$ , the capacitive voltage divider may be left out.





Rev. A1: 23.02.1995

#### **Evaluation Board**

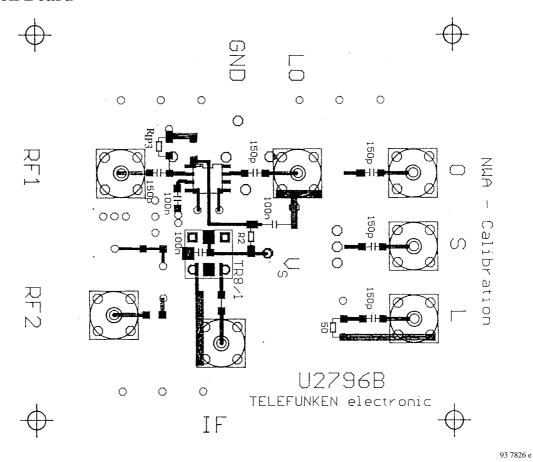
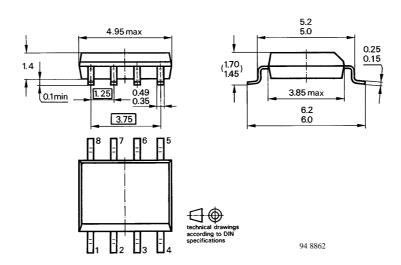


Figure 14.

## **Dimensions in mm**

SO 8 package



#### **Ozone Depleting Substances Policy Statement**

It is the policy of TEMIC TELEFUNKEN microelectronic GmbH to

- 1. Meet all present and future national and international statutory requirements.
- Regularly and continuously improve the performance of our products, processes, distribution and operating systems with respect to their impact on the health and safety of our employees and the public, as well as their impact on the environment.

It is particular concern to control or eliminate releases of those substances into the atmosphere which are known as ozone depleting substances (ODSs).

The Montreal Protocol (1987) and its London Amendments (1990) intend to severely restrict the use of ODSs and forbid their use within the next ten years. Various national and international initiatives are pressing for an earlier ban on these substances.

**TEMIC TELEFUNKEN microelectronic GmbH** semiconductor division has been able to use its policy of continuous improvements to eliminate the use of ODSs listed in the following documents.

- 1. Annex A, B and list of transitional substances of the Montreal Protocol and the London Amendments respectively
- 2. Class I and II ozone depleting substances in the Clean Air Act Amendments of 1990 by the Environmental Protection Agency (EPA) in the USA
- 3. Council Decision 88/540/EEC and 91/690/EEC Annex A, B and C (transitional substances) respectively.

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