

SPEED REGULATOR FOR DC MOTORS

- MATCHING FLEXIBILITY TO MOTORS WITH VARIOUS CHARACTERISTICS
- BUILT-IN CURRENT LIMIT
- ON-CHIP 1.2V REFERENCE VOLTAGE
- STARTING CURRENT: 0.5A @ 2.5V
- REFLECTION COEFFICIENT $K = 20$

The circuit offers an excellent speed regulation with much higher power supply, temperature and load variations than conventional circuits built around discrete components.

The TDA1154 is a monolithic integrated circuit intended for speed regulation of permanent magnet dc motors used in record players, tape recorders, cassette recorders and toys.

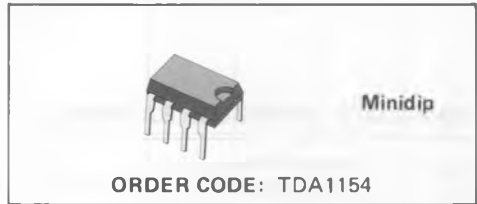
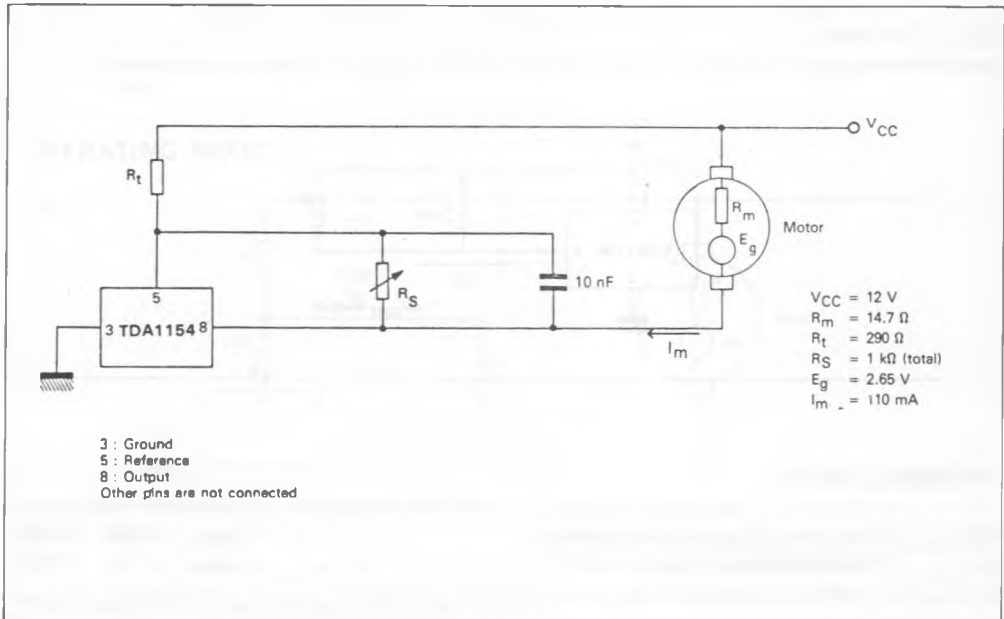
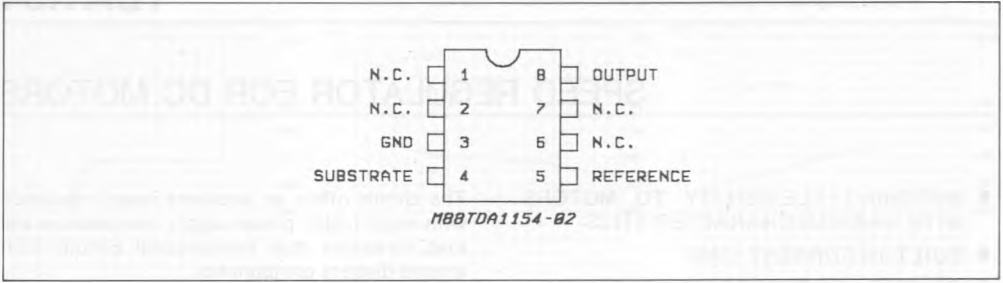


Fig. 1 - Application circuit



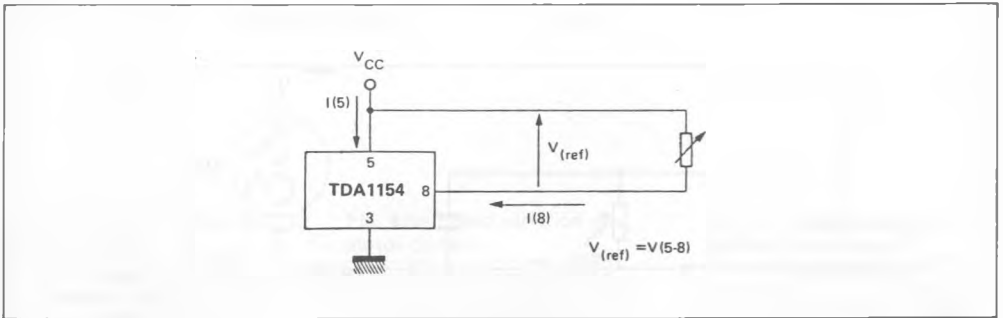
PIN CONNECTION



ABSOLUTE MAXIMUM RATINGS

V_{CC}	Supply voltage	20	V
I_O	Output current	1.2	A
P_{tot}	Power dissipation	(see curve)	W
T_J	Junction temperature	+150	°C
T_{stg}	Storage temperature range	-55 to +150	°C

Fig. 2 - Test circuit



THERMAL DATA

$R_{th J-amb}$	Thermal resistance junction-ambient	max	100	°C/W
$R_{th J-pin 4}$	Thermal resistance junction-pin 4	max	70	°C/W

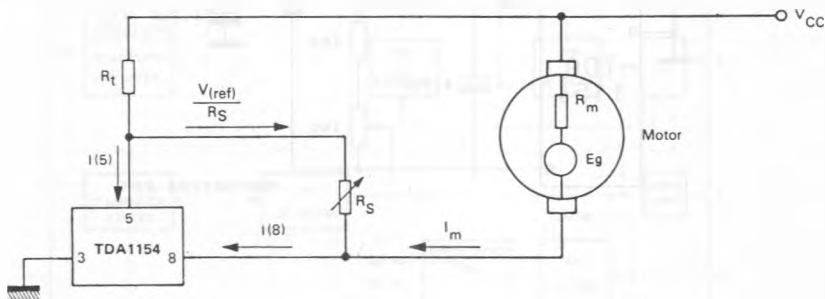
ELECTRICAL CHARACTERISTICS $T_{amb} = +25^{\circ}\text{C}$ (Unless otherwise specified)

Parameter	Test Conditions	Min.	Typ.	Max.	Unit	
$V_{(ref)}$	Reference voltage	$V_{CC} = +6\text{V}$ $I(8) = 0.1\text{A}$	1.15	1.25	1.35	V
$\frac{\Delta V_{(ref)}}{V_{(ref)}} / \Delta T$	Reference voltage temperature coefficient	$V_{CC} = +6\text{V}$ $I(8) = 0.1\text{A}$ $T_{amb} = -20^{\circ}\text{C}$ to $+70^{\circ}\text{C}$	—	0.02	—	%/°C
$\frac{\Delta V_{(ref)}}{V_{(ref)}} / \Delta V_{CC}$	Line regulator	$V_{CC} = +4\text{V}$ to $+18\text{V}$ $I(8) = 0.1\text{A}$	—	0.02	—	%/V
$\frac{\Delta V_{(ref)}}{V_{(ref)}} / \Delta I(8)$	Load regulator	$V_{CC} = +6\text{V}$ $I(8) = 25$ to 400mA	—	0.009	—	%/mA
$V(5-3)$	Minimum supply voltage	$I(8) = 0.1\text{A}$ $\frac{\Delta V_{(ref)}}{V_{(ref)}} = -5\%$	2.5	—	—	V
$I(8)$	Starting current(*)	$\frac{\Delta V_{(ref)}}{V_{(ref)}} = -50\%$ $V_{CC} = +5\text{V}$ $V_{CC} = +2.5\text{V}$	1.2 0.5	— 0.8	—	A
$I_O(5)$	Quiescent current on pin 5	$V_{CC} = +6\text{V}$ $I(8) = 100\ \mu\text{A}$	—	1.7	—	mA
K	$K = \frac{\Delta I(8)}{\Delta I(5)}$ reflection coefficient	$V_{CC} = +6\text{V}$ $I(8) = 0.1\text{A}$	18	20	22	
$\frac{\Delta K}{K} / \Delta V_{CC}$	K spread versus V_{CC}	$V_{CC} = +6\text{V}$ to $+18\text{V}$ $I(8) = 0.1\text{A}$	—	0.45	—	%/V
$\frac{\Delta K}{K} / \Delta I(8)$	K spread versus $I(8)$	$V_{CC} = +6\text{V}$ $I(8) = 25$ to 400mA	—	0.005	—	%/mA
$\frac{\Delta K}{K} / \Delta T$	K spread versus temperature	$V_{CC} = +6\text{V}$ $I(8) = 0.1\text{A}$ $T_{amb} = +20^{\circ}\text{C}$ to $+70^{\circ}\text{C}$	—	0.02	—	%/°C

(*) An internal protection circuit reduces the current if the temperature of the junction increase: $I(8) = 0.75\text{A}$ at $T_j = +140^{\circ}\text{C}$.

OPERATING MODE

Fig. 3



The circuit maintains a 1.2V constant reference voltage between pins 5 and 8:

$$V(5-8) = V_{(ref)} = 1.2\text{V}$$

The current $I(5)$ drawn by the circuit at pin 5 is

sum of two currents.

One is constant: $I_O(5) = 1.7\text{mA}$ and the other is proportional to pin 8 current $I(8)$:

$$I(5) = I_O(5) + I(8)K \quad (I_O(5) = 1.7\text{mA}, K = 20)$$

If E_g and R_m are motor back electromotive force and motor internal resistance respectively, then:

$$E_g + R_m I_m = R_t \left[I(5) + \frac{V_{(ref)}}{R_s} \right] + V_{(ref)} \quad (b)$$

From figure 2 it is seen that:

$$I(8) = I_m + \frac{V_{(ref)}}{R_s} \quad (c)$$

Substituting equations (a) and (c) into (b) yields:

$$E_g = I_m \left[\frac{R_t}{K} - R_m \right] + \quad (1)$$

$$+ V_{(ref)} \left[\frac{R_t}{R_s} \left(1 + \frac{1}{K} \right) + 1 \right] + R_t I_O(5) \quad (2)$$

The motor speed will be independent of the resisting torque if E_g is also independent of I_m . Therefore, in order to determine the value of R_t term (1) in (d) must be zero:

$$R_t = K R_m \quad (K = 20)$$

If $R_t > K R_m$, an instability may occur as a result of overcompensation.

The value of R_s is determined by term (2) in (d) so as to obtain the back electromotive force (E_g) corresponding to required motor speed:

$$R_s = R_t \frac{V_{(ref)} (1 + 1/K)}{E_g - V_{(ref)} - R_t I_O(5)} \cong$$

$$\cong R_t \frac{V_{(ref)}}{E_g - V_{(ref)} - R_t I_O(5)}$$

Where $V_{(ref)} = 1.2V$ and $I_O(5) = 1.7 mA$

Fig. 4 - Application circuit

