

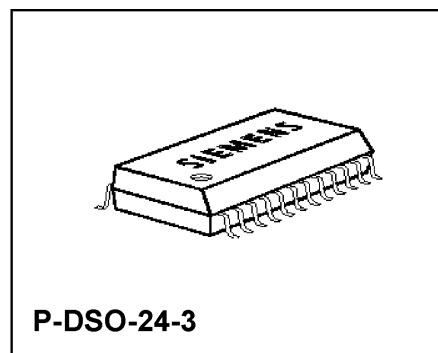
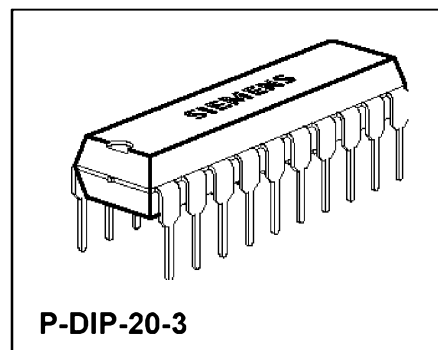
2-Phase Stepper-Motor Driver

TCA 3727

Bipolar IC

Features

- 2 x 0.75 amp. / 50 V outputs
- Integrated driver, control logic and current control (chopper)
- Fast free-wheeling diodes
- Max. supply voltage 52 V
- Outputs free of crossover current
- Offset-phase turn-ON of output stages
- Z-diode for logic supply
- Low standby-current drain
- Full, half, quarter, mini, quasi-sine step

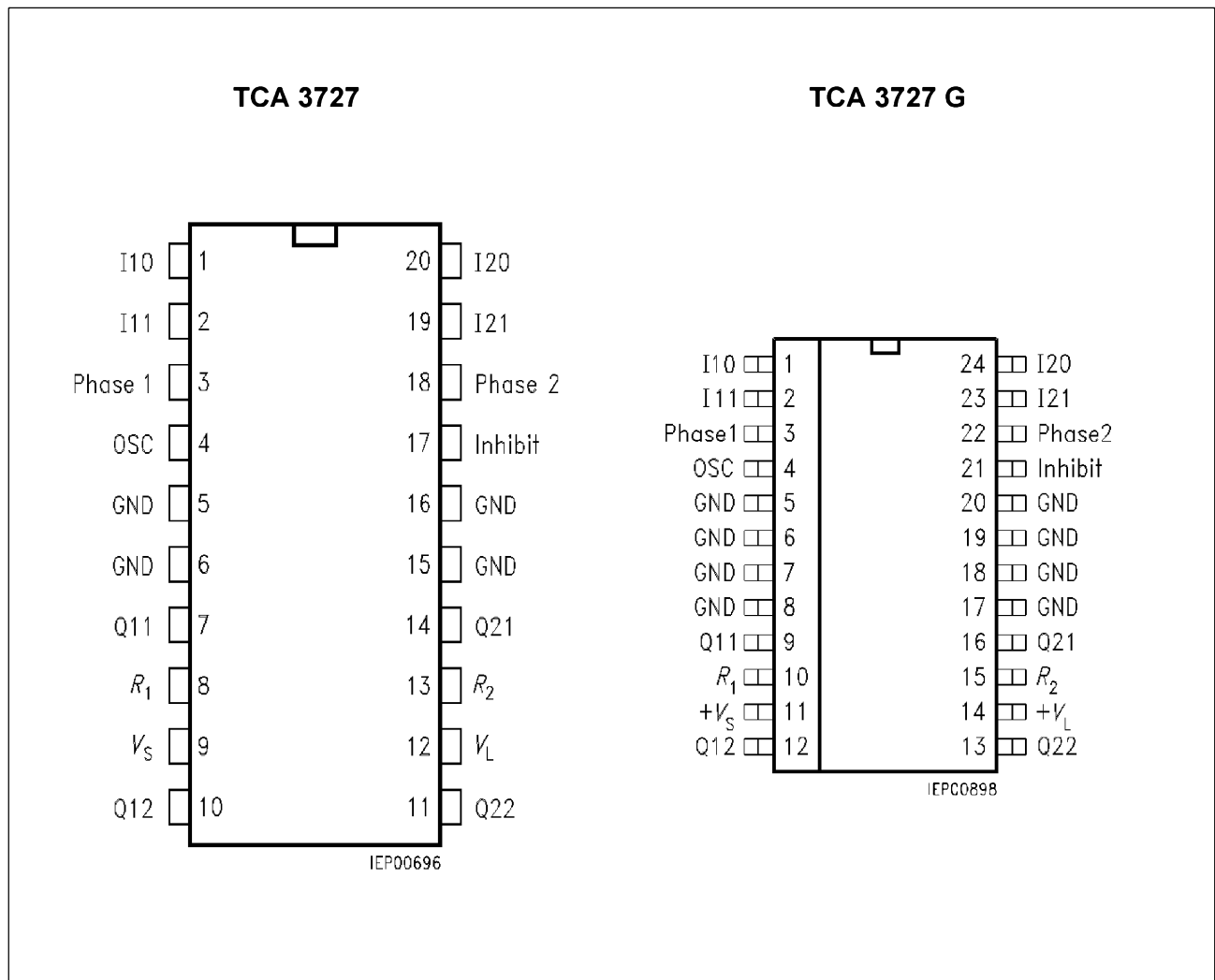


Type	Ordering Code	Package
TCA 3727	Q67000-A8302	P-DIP-20-3
TCA 3727 G	Q67000-A8335	P-DSO-24-3 (SMD)

TCA 3727 is a bipolar, monolithic IC for driving bipolar stepper motors, DC motors and other inductive loads that operate on constant current. The control logic and power output stages for two bipolar windings are integrated on a single chip which permits switched current control of motors with 0.75 A per phase at operating voltages up to 50 V.

The direction and value of current are programmed for each phase via separate control inputs. A common oscillator generates the timing for the current control and turn-on with phase offset of the two output stages. The two output stages in a full-bridge configuration have integrated, fast free-wheeling diodes and are free of crossover current. The logic is supplied either separately with 5 V or taken from the motor supply voltage by way of a series resistor and an integrated Z-diode. The device can be driven directly by a microprocessor with the possibility of all modes from full step through half step to mini step.

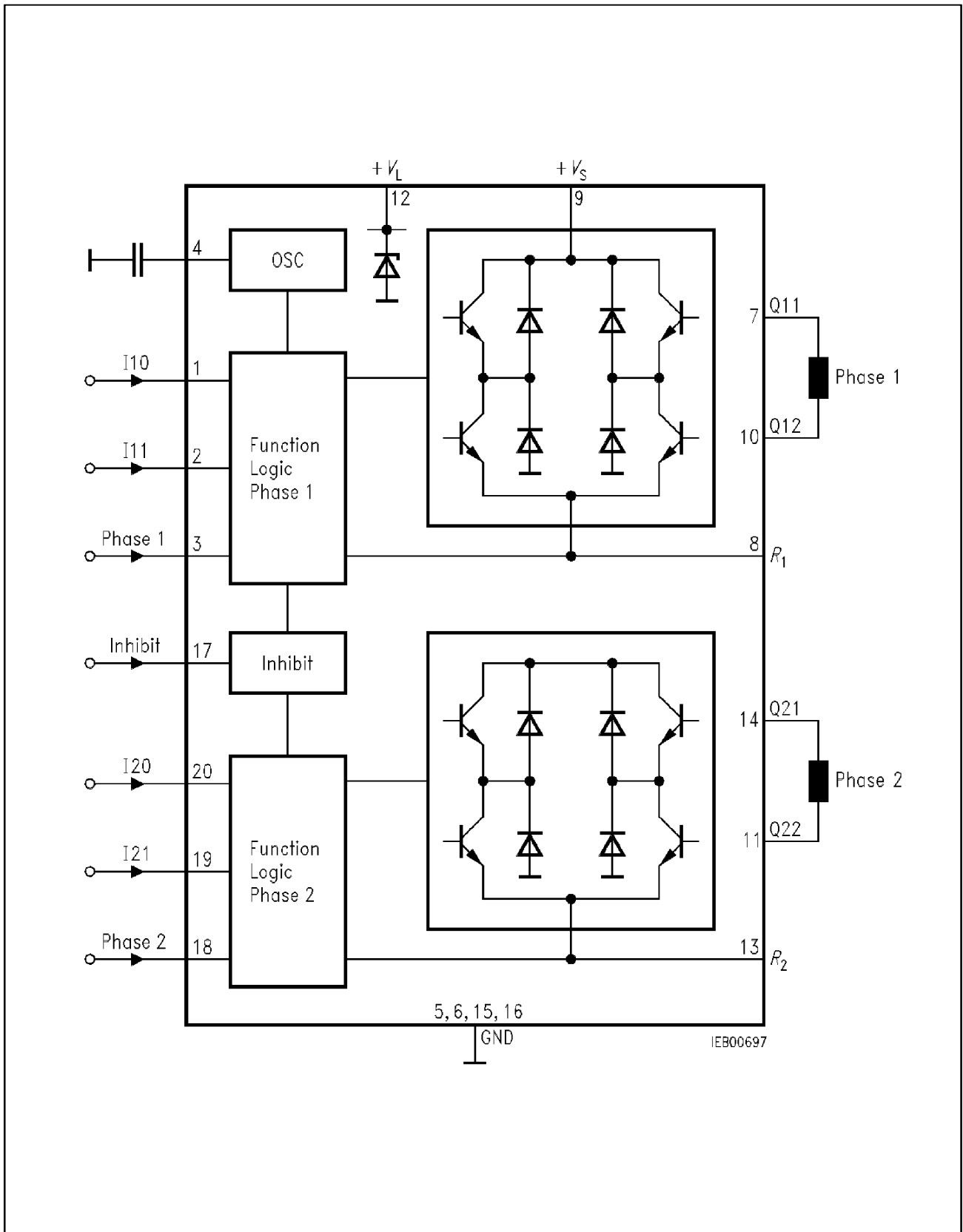
Pin Configuration (top view)



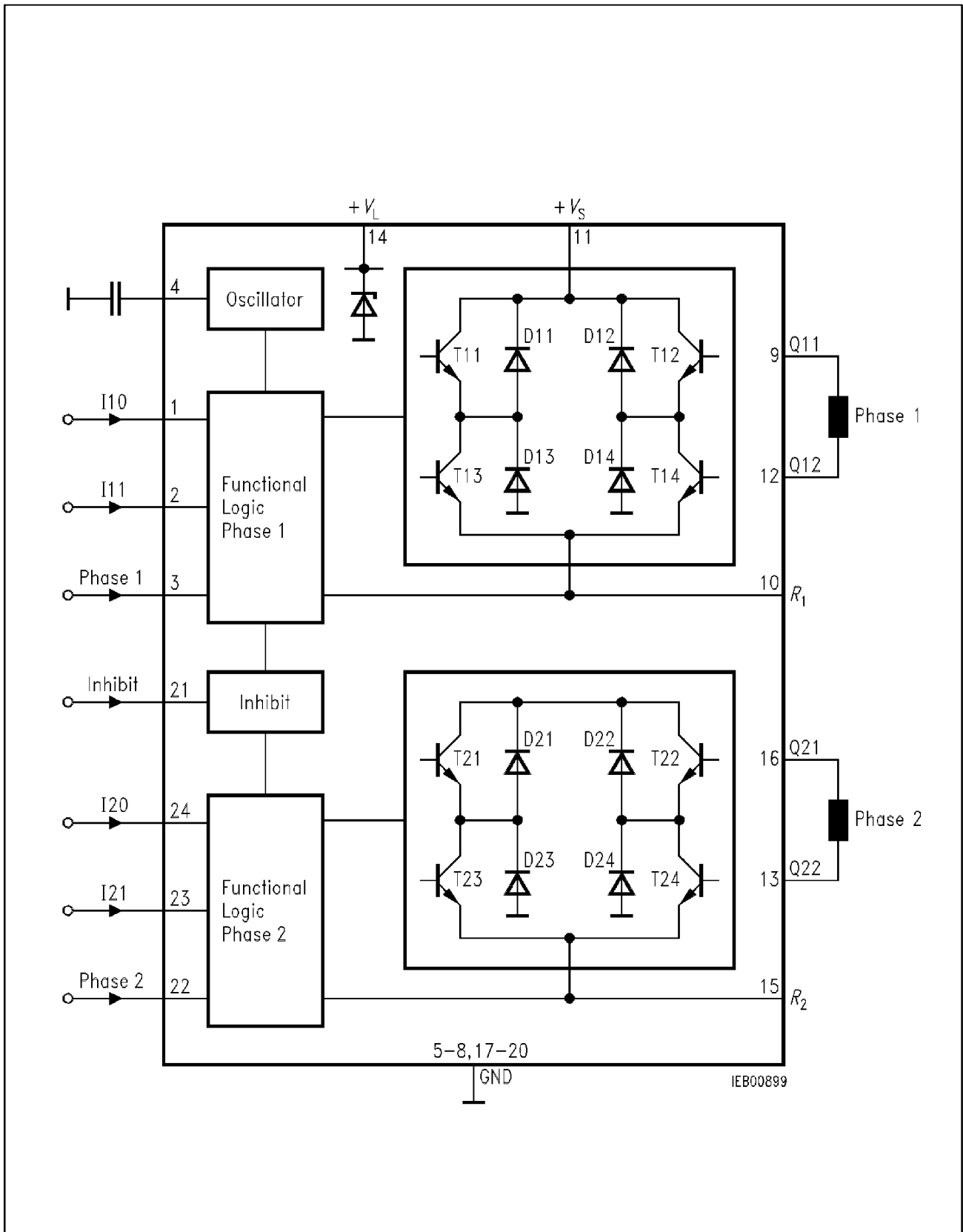
Pin Definitions and Functions

Pin	Function																				
1, 2, 19, 20 (1, 2, 23, 24) ¹⁾	<p>Digital control inputs IX0, IX1 for the magnitude of the current of the particular phase.</p> <table border="1"> <thead> <tr> <th>IX1</th> <th>IX0</th> <th>Phase current</th> <th>Example of motor status</th> </tr> </thead> <tbody> <tr> <td>H</td> <td>H</td> <td>0</td> <td>No current</td> </tr> <tr> <td>H</td> <td>L</td> <td>$1/3 I_{max}$</td> <td>Hold</td> </tr> <tr> <td>L</td> <td>H</td> <td>$2/3 I_{max}$</td> <td>Normal mode</td> </tr> <tr> <td>L</td> <td>L</td> <td>I_{max}</td> <td>Accelerate</td> </tr> </tbody> </table> <p style="text-align: right;">typical I_{max} with $R_{sense} = 1 \Omega : 750 \text{ mA}$</p>	IX1	IX0	Phase current	Example of motor status	H	H	0	No current	H	L	$1/3 I_{max}$	Hold	L	H	$2/3 I_{max}$	Normal mode	L	L	I_{max}	Accelerate
IX1	IX0	Phase current	Example of motor status																		
H	H	0	No current																		
H	L	$1/3 I_{max}$	Hold																		
L	H	$2/3 I_{max}$	Normal mode																		
L	L	I_{max}	Accelerate																		
3	Input Phase 1 ; controls the current through phase winding 1. On H-potential the phase current flows from Q11 to Q12, on L-potential in the reverse direction.																				
5, 6, 15, 16 (5, 6, 7, 8, 17, 18, 19, 20) ¹⁾	Ground ; all pins are connected internally.																				
4	Oscillator ; works at approx. 25 kHz if this pin is wired to ground across 2.2 nF.																				
8 (10) ¹⁾	Resistor R_1 for sensing the current in phase 1.																				
7, 10 (9, 12) ¹⁾	Push-pull outputs Q11, Q12 for phase 1 with integrated free-wheeling diodes.																				
9 (11) ¹⁾	Supply voltage ; block to ground, as close as possible to the IC, with a stable electrolytic capacitor of at least 10 μF in parallel with a ceramic capacitor of 220 nF.																				
12 (14) ¹⁾	Logic supply voltage ; either supply with 5 V or connect to + V_S across a series resistor. A Z-diode of approx. 7 V is integrated. In both cases block to ground directly on the IC with a stable electrolytic capacitor of 10 μF in parallel with a ceramic capacitor of 100 nF.																				
11, 14 (13, 16) ¹⁾	Push-pull outputs Q22, Q21 for phase 2 with integrated free wheeling diodes.																				
13 (15) ¹⁾	Resistor R_2 for sensing the current in phase 2.																				
17 (21) ¹⁾	Inhibit input ; the IC can be put on standby by low potential on this pin. This reduces the current consumption substantially.																				
18 (22) ¹⁾	Input phase 2 ; controls the current flow through phase winding 2. On H-potential the phase current flows from Q21 to Q22, on L potential in the reverse direction.																				

1) TCA 3727 G only



Block Diagram
TCA 3727



Block Diagram
TCA 3727 G

Absolute Maximum Ratings

$T_A = -40$ to 125 °C

Parameter	Symbol	Limit Values		Unit	Remarks
		min.	max.		
Supply voltage	V_S	0	52	V	–
Logic supply voltage	V_L	0	6.5	V	Z-diode
Z-current of V_L	I_L	–	50	mA	–
Output current	I_Q	–	1	A	–
Ground current	I_{GND}	–	2	A	–
Logic inputs	V_{Ixx}	–6	$V_L + 0.3$	V	I_{xx} ; Phase 1, 2; Inhibit
R_1, R_2 , oscillator input voltage	V_{RX}, V_{OSC}	–0.3	$V_L + 0.3$	V	–
Diode currents to + V_S	I_{F+}	–	1	A	–
to ground	I_{F-}	–	1	A	–
Junction temperature	T_j	–	125	°C	–
	T_j	–	150	°C	max. 10,000 h
Storage temperature	T_{stg}	50	125	°C	–

Operating Range

Parameter	Symbol	Limit Values		Unit	Remarks
		min.	max.		
Supply voltage	V_S	5	50	V	–
Logic supply voltage	V_L	4.5	6.5	V	without series resistor
Case temperature	T_C	– 40	110	°C	measured on pin 5 $P_{diss} = 2\text{ W}$
Output current	I_Q	–	1000	mA	–
Logic inputs	V_{IXX}	– 5	V_L	V	I_{XX} ; Phase 1, 2; Inhibit
Thermal resistances					
system-air	$R_{th\ SA}$	–	56	K/W	P-DIP-20-3
system-air (soldered on a 35 μm thick 20 cm^2 PC board copper area)	$R_{th\ SA}$	–	40	K/W	P-DIP-20-3
system-case	$R_{th\ SC}$	–	18	K/W	measured on pin 5 P-DIP-20-3
system-air	$R_{th\ SA}$	–	75	K/W	P-DSO-24-3
system-air (soldered on a 35 μm thick 20 cm^2 PC board copper area)	$R_{th\ SA}$	–	50	K/W	P-DSO-24-3
system-case	$R_{th\ SC}$	–	15	K/W	measured on pin 5 P-DSO-24-3

Characteristics

$V_S = 40 \text{ V}$; $V_L = 5 \text{ V}$; $-25 \text{ }^\circ\text{C} \leq T_j \leq 125 \text{ }^\circ\text{C}$

Parameter	Symbol	Limit Values			Unit	Test Condition
		min.	typ.	max.		

Current Consumption

from + V_S	I_S	–	0.2	0.5	mA	$V_{inh} = L$
from + V_S	I_S	–	16	20	mA	$V_{inh} = H$
from + V_L	I_L	–	1.7	3.0	mA	$I_{Q1/2} = 0, I_{XX} = L$ $V_{inh} = L$
from + V_L	I_L	–	18	25	mA	$V_{inh} = H$ $I_{Q1/2} = 0, I_{XX} = L$

Oscillator

Output charging current	I_{OSC}	–	110	–	μA	
Charging threshold	V_{OSCL}	–	1.3	–	V	
Discharging threshold	V_{OSCH}	–	2.3	–	V	
Frequency	f_{OSC}	18	25	35	kHz	$C_{OSC} = 2.2 \text{ nF}$

Phase Current Selection (R_1, R_2)

Current Limit Threshold

No current	V_{sense}	–	0	–	mV	$IX0 = H; IX1 = H$
Hold	V_{sense}	200	250	300	mV	$IX0 = L; IX1 = H$
Setpoint	V_{sense}	460	540	620	mV	$IX0 = H; IX1 = L$
Accelerate	V_{sense}	740	825	910	mV	$IX0 = L; IX1 = L$

Logic Inputs

(I_{X1} ; I_{X0} ; phase x; inhibit)

Threshold (I_{XX} , Phase X)	V_1	1.4 (H→L)	–	2.3 (L→H)	V	–
L-input current (logic inputs)	I_{LInh}	– 10	–	–	μA	$V_1 = 1.4 \text{ V}$
L-input current (i_{X1}, i_{X0} , phase)	I_{iL}	– 100	–	–	μA	$V_1 = 0 \text{ V}$
H-input current	I_{iH}	–	–	10	μA	$V_1 = 5 \text{ V}$

Standby Cutout (inhibit)

Threshold	$V_{inh} (L \rightarrow H)$	2.0	3.0	4.0	V	$V_L = 5 \text{ V}$
Threshold	$V_{inh} (H \rightarrow L)$	1.7	2.3	2.9	V	$V_L = 5 \text{ V}$
Hysteresis	V_{inhhy}	0.3	0.7	1.1	V	$V_L = 5 \text{ V}$

Internal Z-Diode

Z-voltage	V_{LZ}	6.5	7.4	8.2	V	$I_L = 50 \text{ mA}$
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Characteristics (cont'd)

$V_S = 40 \text{ V}$; $V_L = 5 \text{ V}$; $-25 \text{ °C} \leq T_j \leq 125 \text{ °C}$

Parameter	Symbol	Limit Values			Unit	Test Condition
		min.	typ.	max.		

Power Outputs

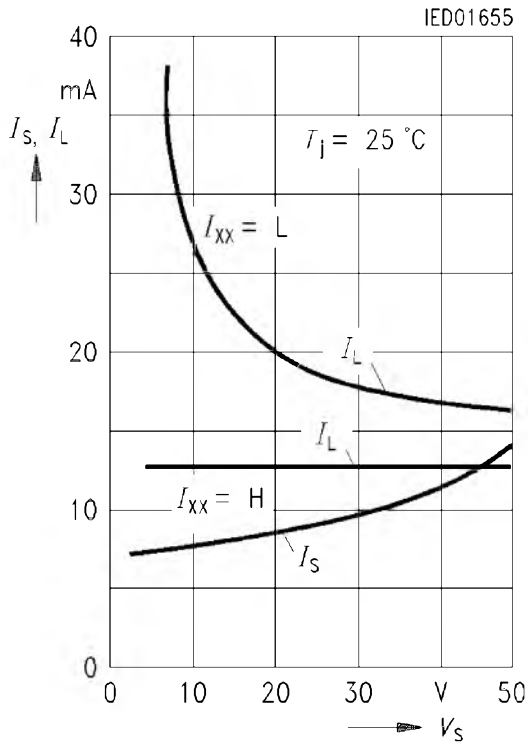
Diode Transistor Sink Pair (D13, T13; D14, T14; D23, T23; D24, T24)

Saturation voltage	V_{satI}	–	0.3	0.6	V	$I_Q = -0.5 \text{ A}$
Saturation voltage	V_{satI}	–	0.5	1.0	V	$I_Q = -0.75 \text{ A}$
Reverse current	I_{RI}	–	–	300	μA	$V_Q = 40 \text{ V}$
Forward voltage	V_{FI}	–	0.9	1.3	V	$I_Q = 0.5 \text{ A}$
Forward voltage	V_{FI}	–	1.0	1.4	V	$I_Q = 0.75 \text{ A}$

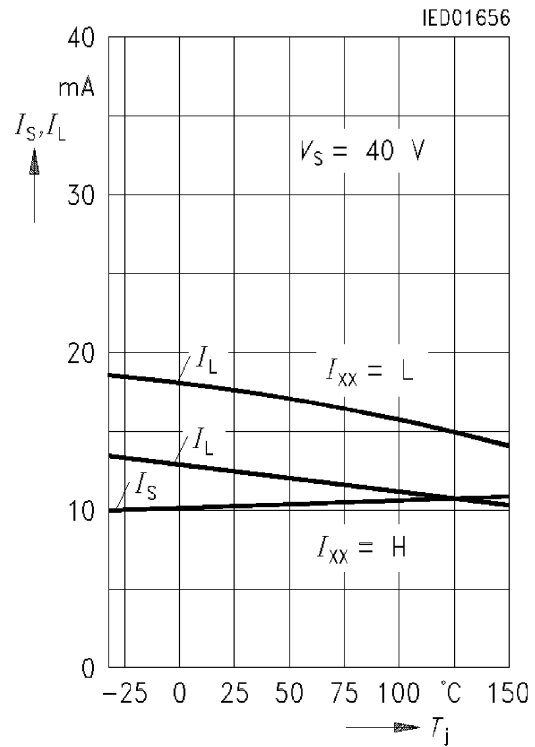
Diode Transistor Source Pair (D11, T11; D12, T12; D21, T21; D22, T22)

Saturation voltage	V_{satuC}	–	0.9	1.2	V	$I_Q = 0.5 \text{ A}$; charge
Saturation voltage	V_{satuD}	–	0.3	0.7	V	$I_Q = 0.5 \text{ A}$; discharge
Saturation voltage	V_{satuC}	–	1.1	1.4	V	$I_Q = 0.75 \text{ A}$; charge
Saturation voltage	V_{satuD}	–	0.5	1.0	V	$I_Q = 0.75 \text{ A}$; discharge
Reverse current	I_{Ru}	–	–	300	μA	$V_Q = 0 \text{ V}$
Forward voltage	V_{Fu}	–	1.0	1.3	V	$I_Q = -0.5 \text{ A}$
Forward voltage	V_{Fu}	–	1.1	1.4	V	$I_Q = -0.75 \text{ A}$
Diode leakage current	I_{SL}	–	1	2	mA	$I_F = -0.75 \text{ A}$

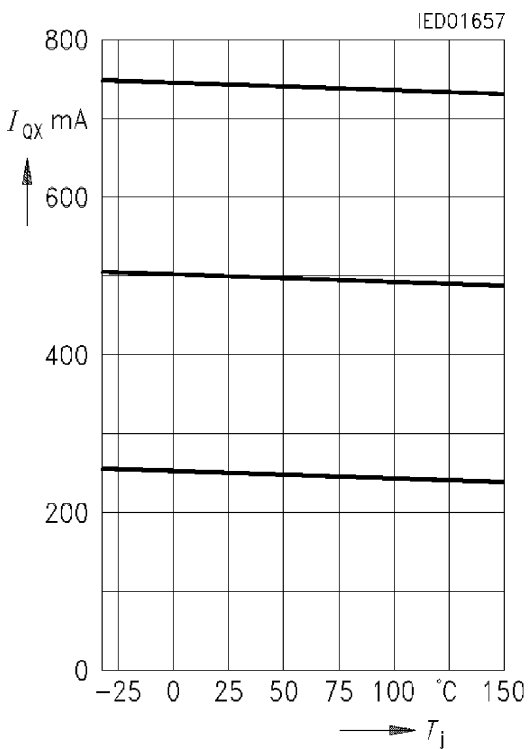
Quiescent Current I_S, I_L versus Supply Voltage V_S



Quiescent Current I_S, I_L versus Junction Temperature T_j



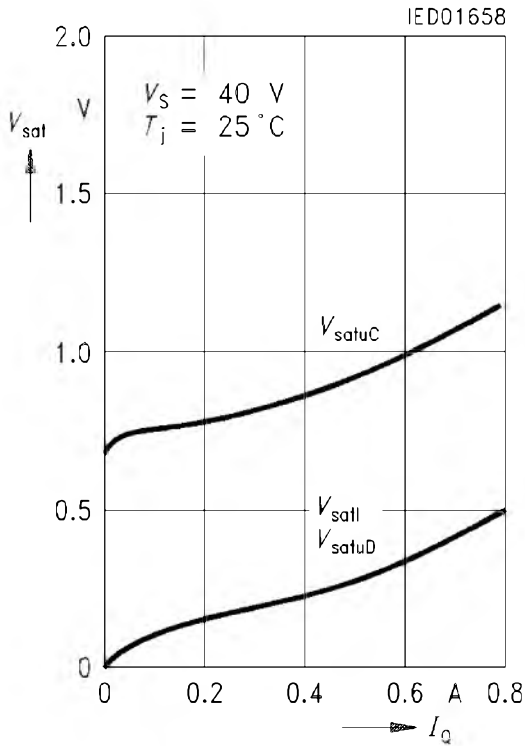
Output Current I_{QX} versus Junction Temperature T_j



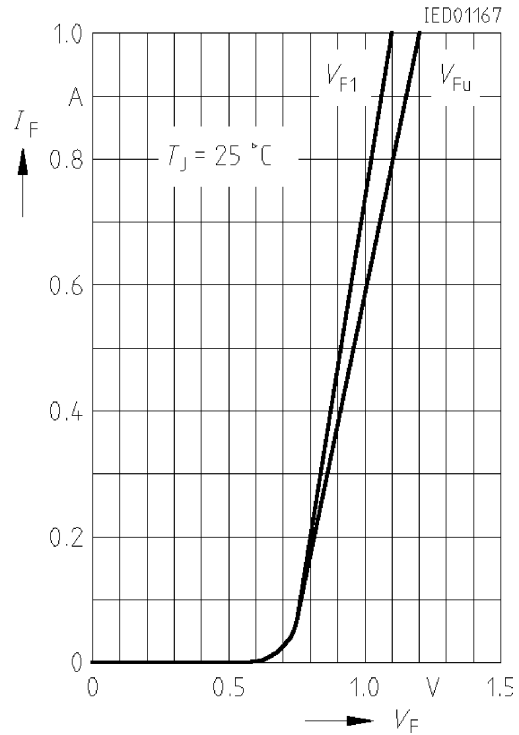
Operating Condition:

- $V_L = 5\text{ V}$
- $V_{inh} = H$
- $C_{OSC} = 2.2\text{ nF}$
- $R_{sense} = 1\text{ }\Omega$
- Load: $L = 10\text{ mH}$
 $R = 2.4\text{ }\Omega$
- $f_{phase} = 50\text{ Hz}$
- mode: fullstep

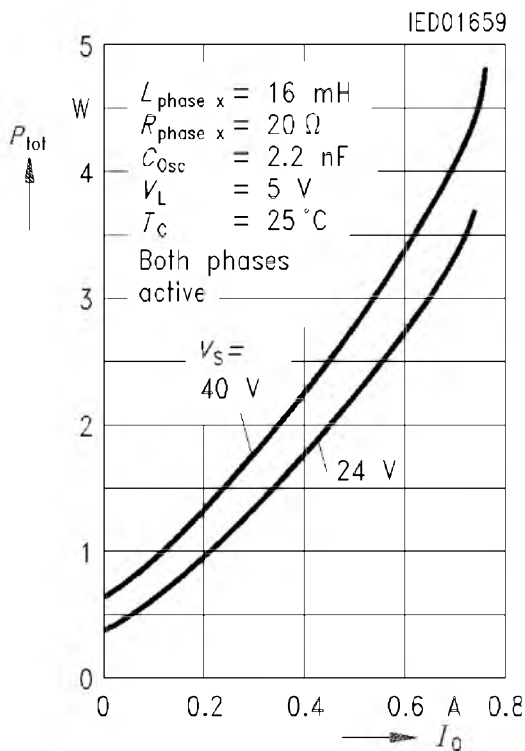
Output Saturation Voltages V_{sat} versus Output Current I_Q



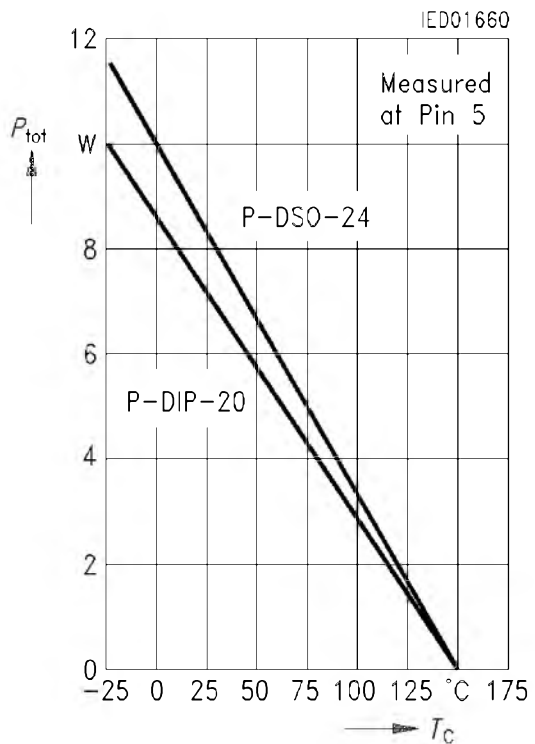
Forward Current I_F of Free-Wheeling Diodes versus Forward Voltages V_F



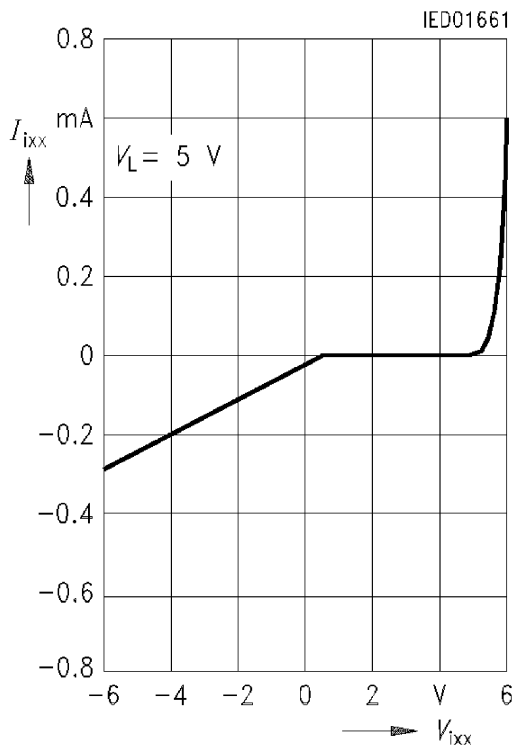
Typical Power Dissipation P_{tot} versus Output Current I_Q (Non Stepping)



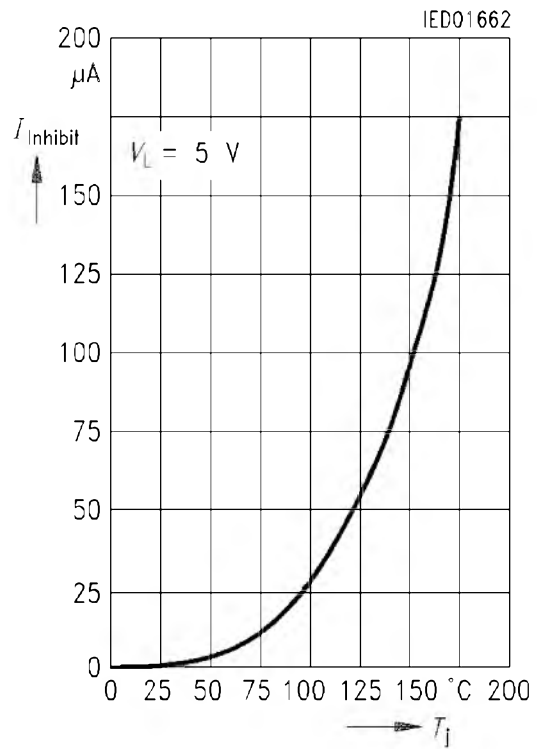
Permissible Power Dissipation P_{tot} versus Case Temperature T_C



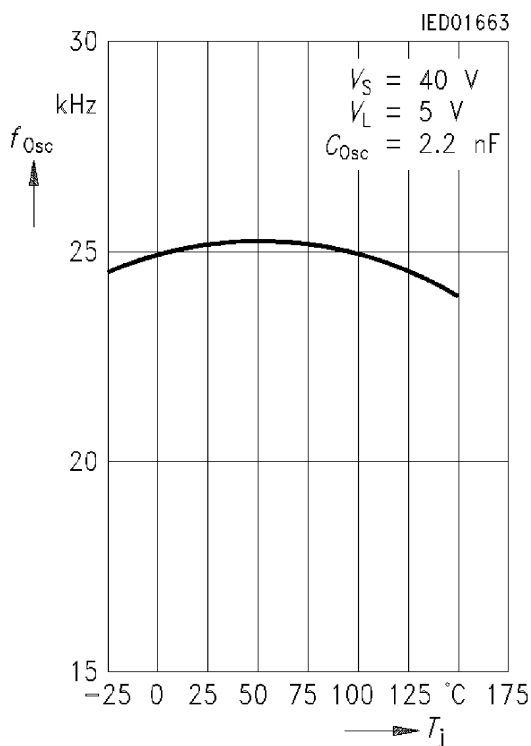
Input Characteristics of I_{ixx} , Phase X, Inhibit

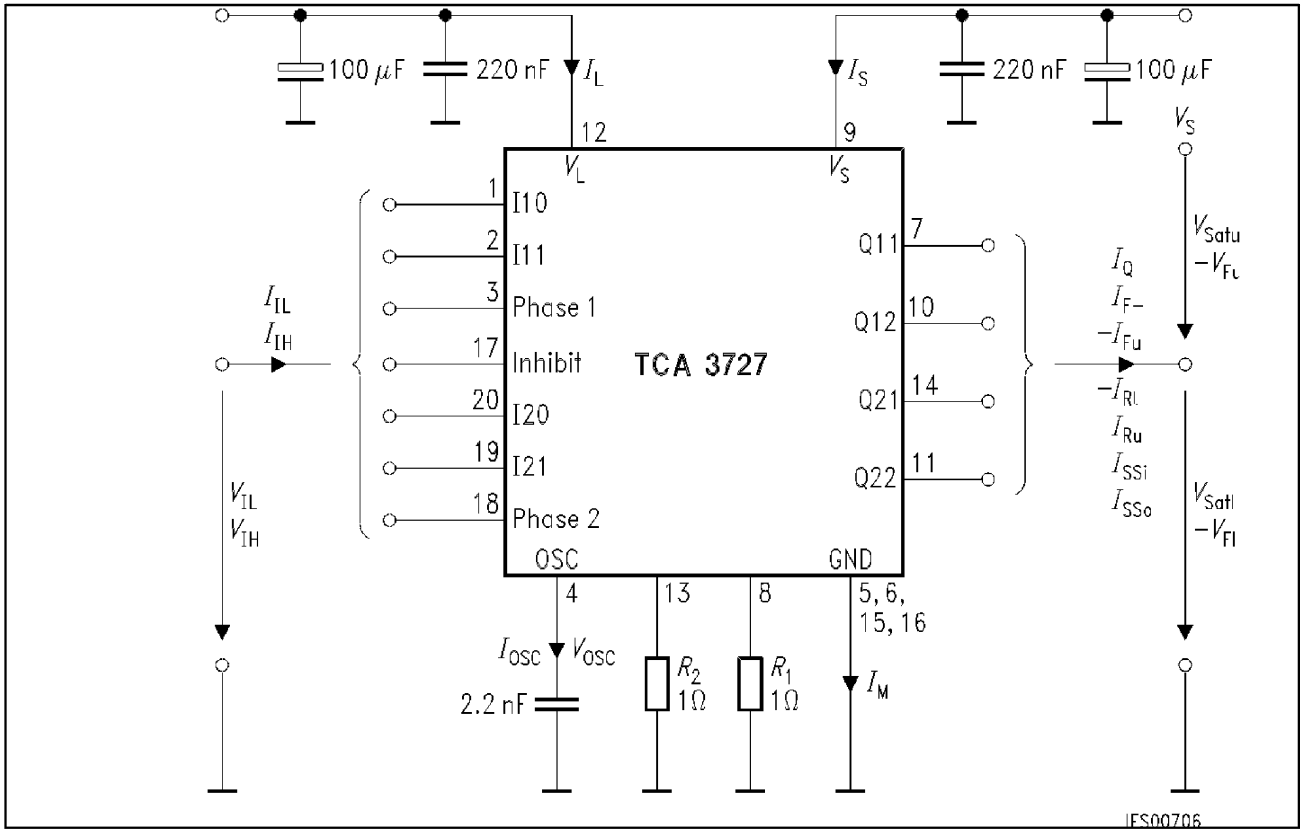


Input Current of Inhibit versus Junction Temperature T_j



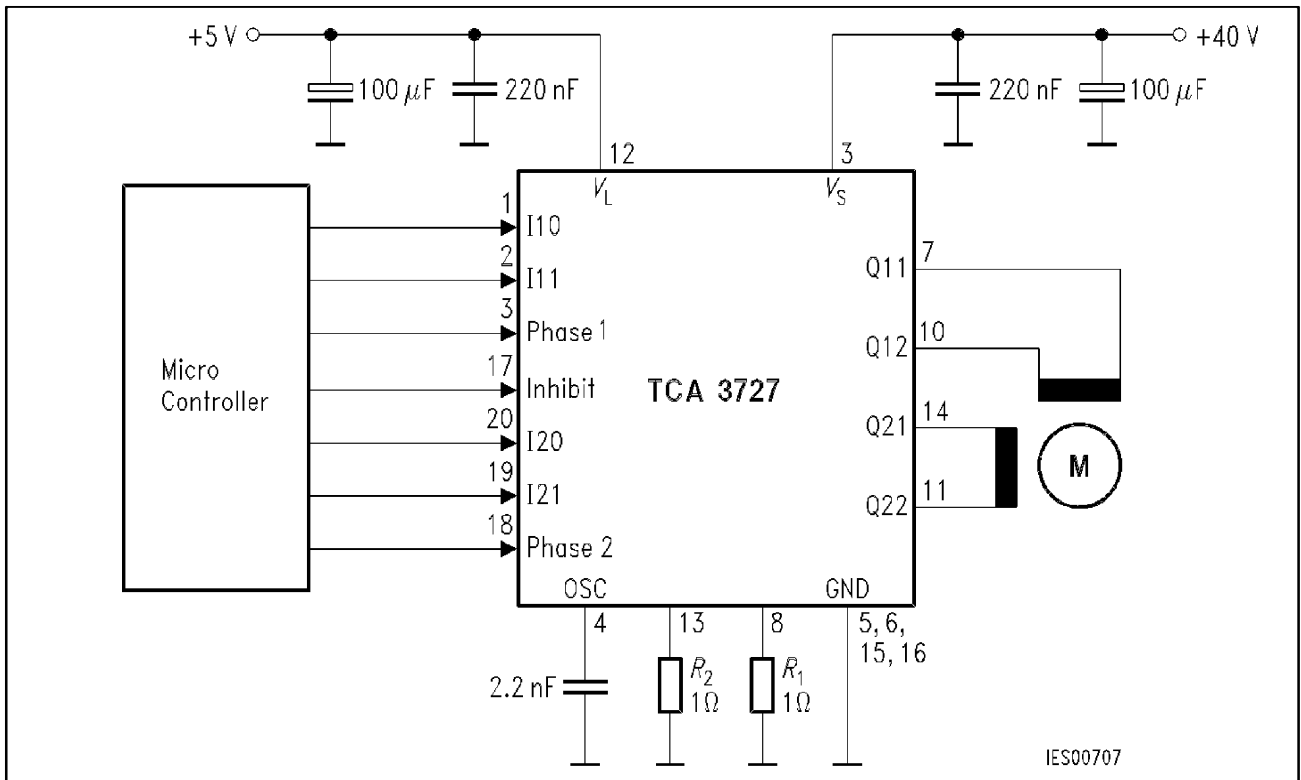
Oscillator Frequency f_{osc} versus Junction Temperature T_j





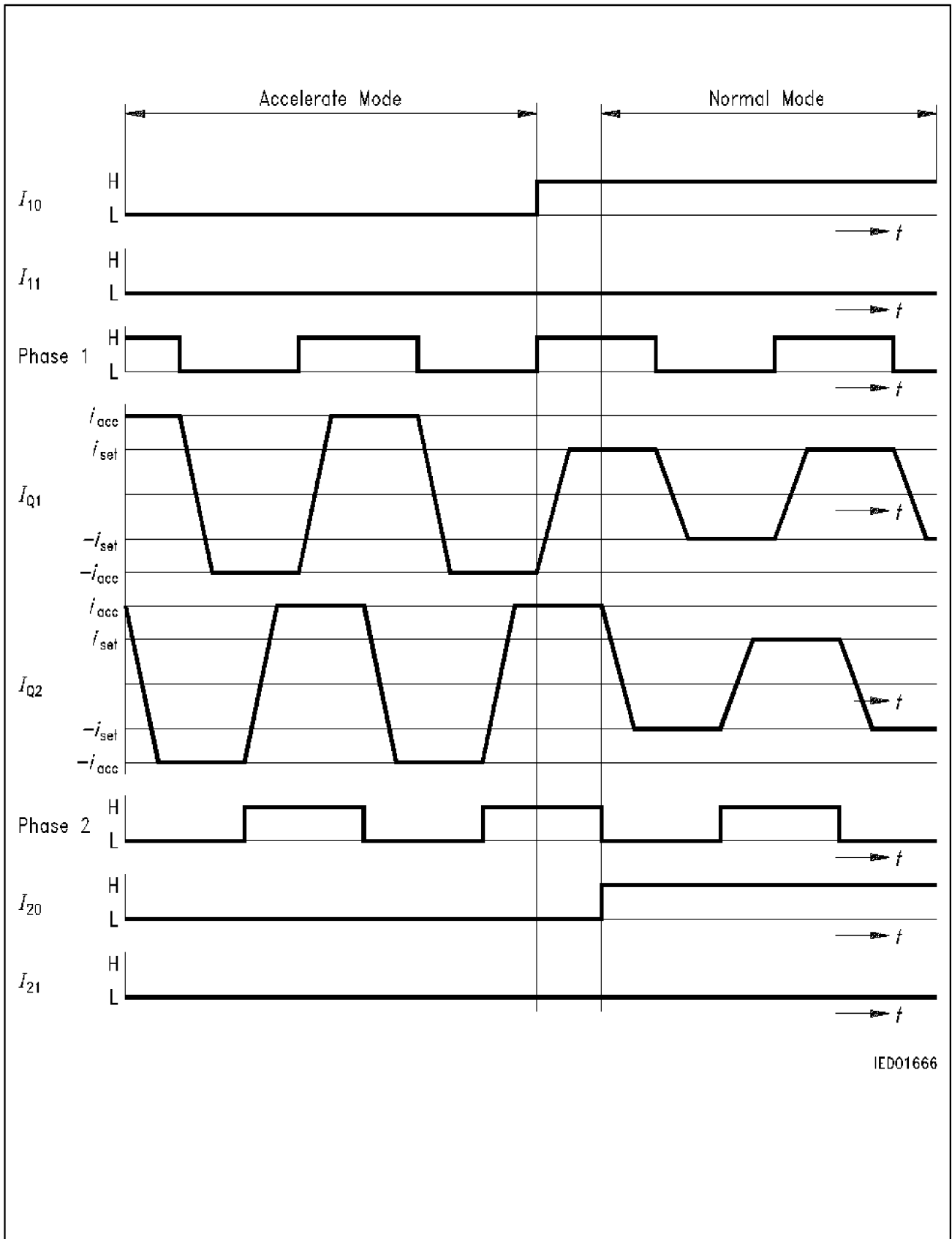
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Test Circuit



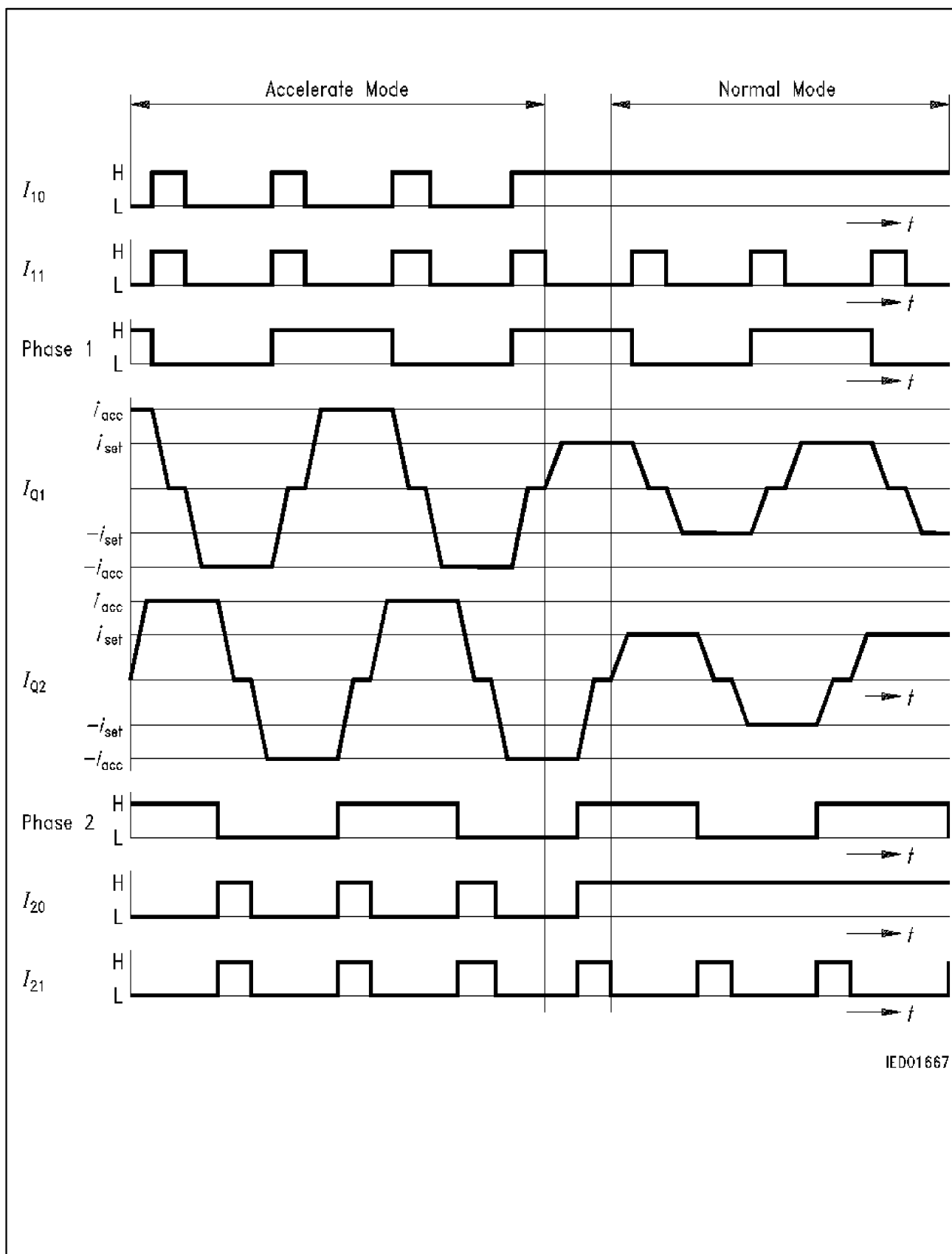
IES00707

Application Circuit

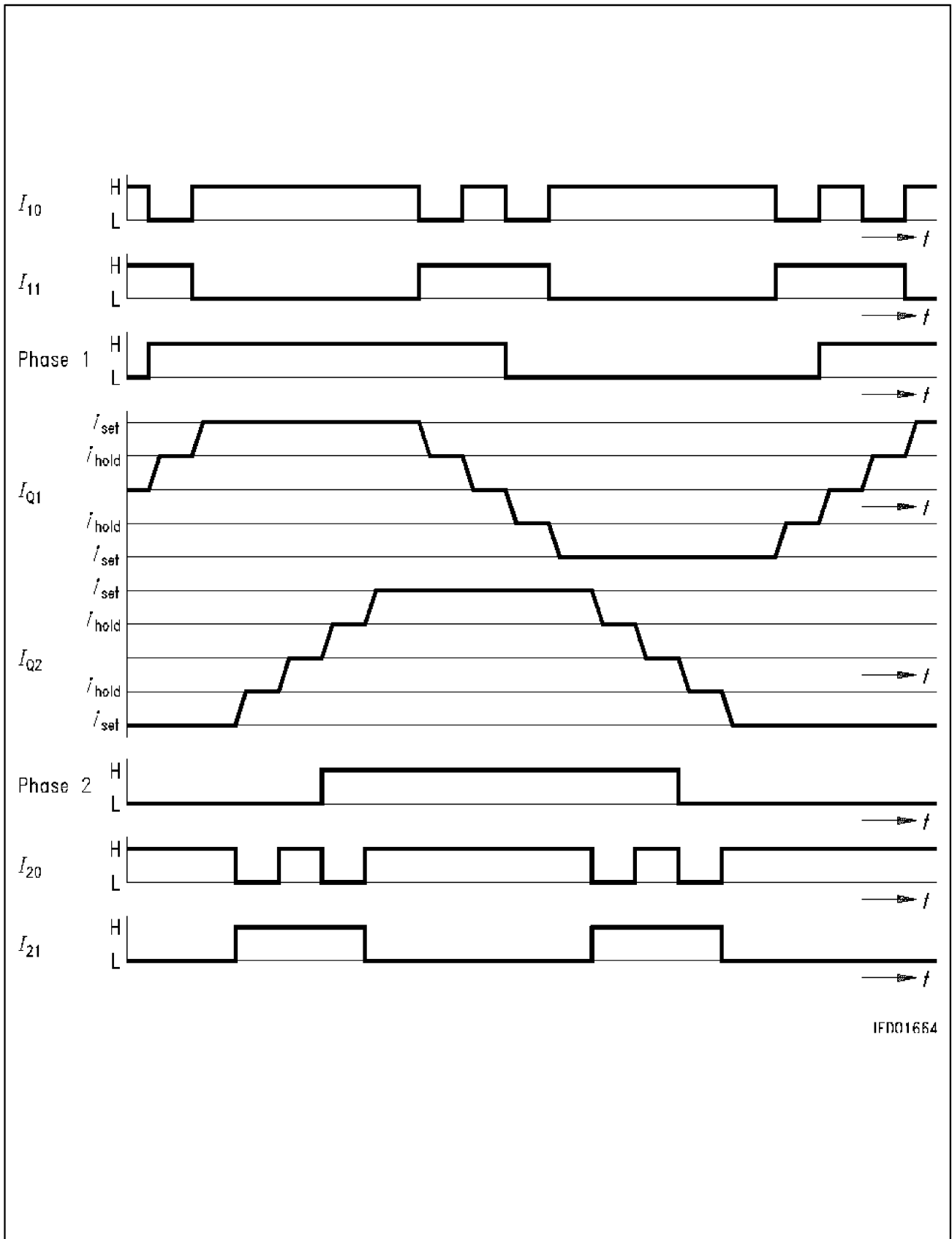


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Full-Step Operation

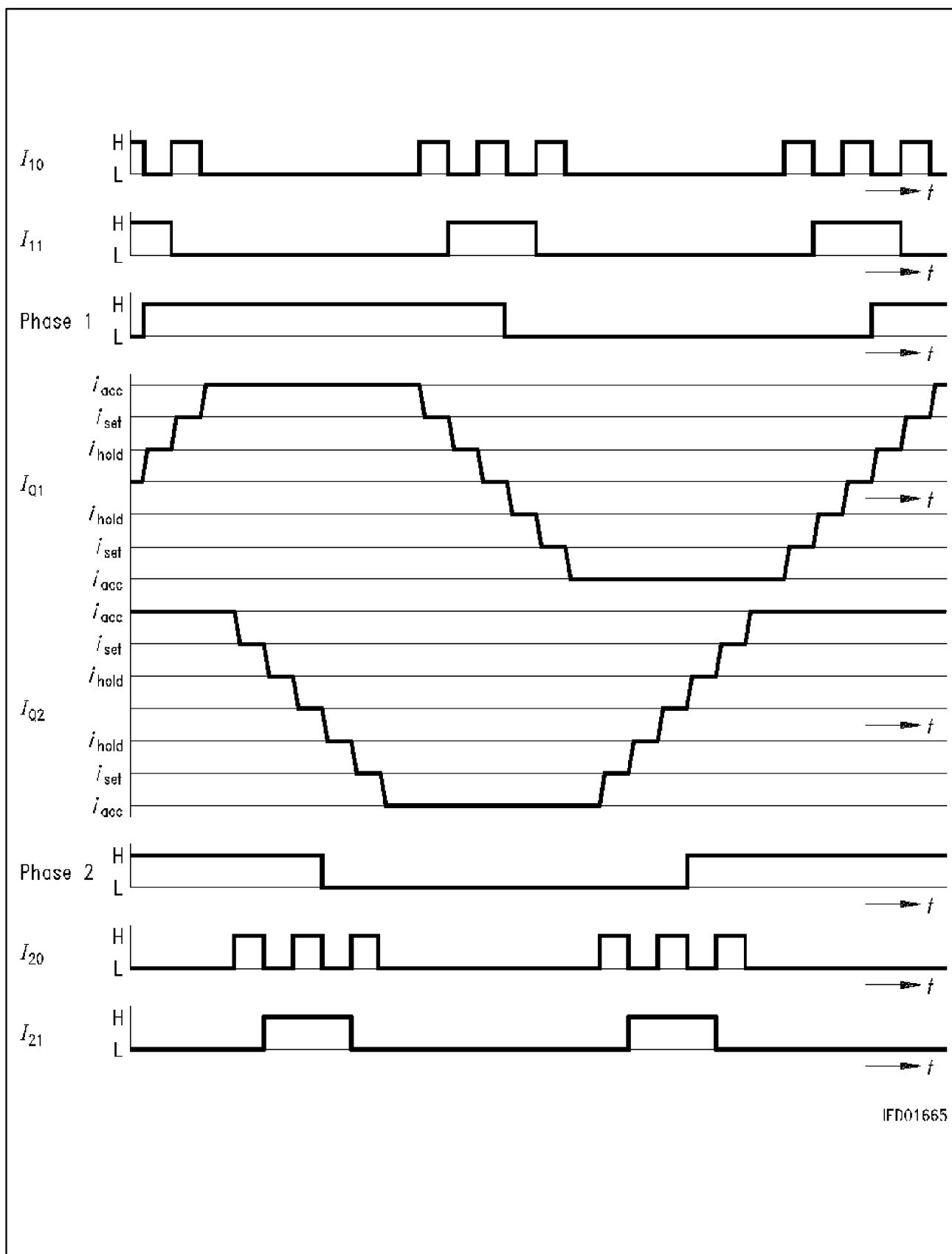


Half-Step Operation

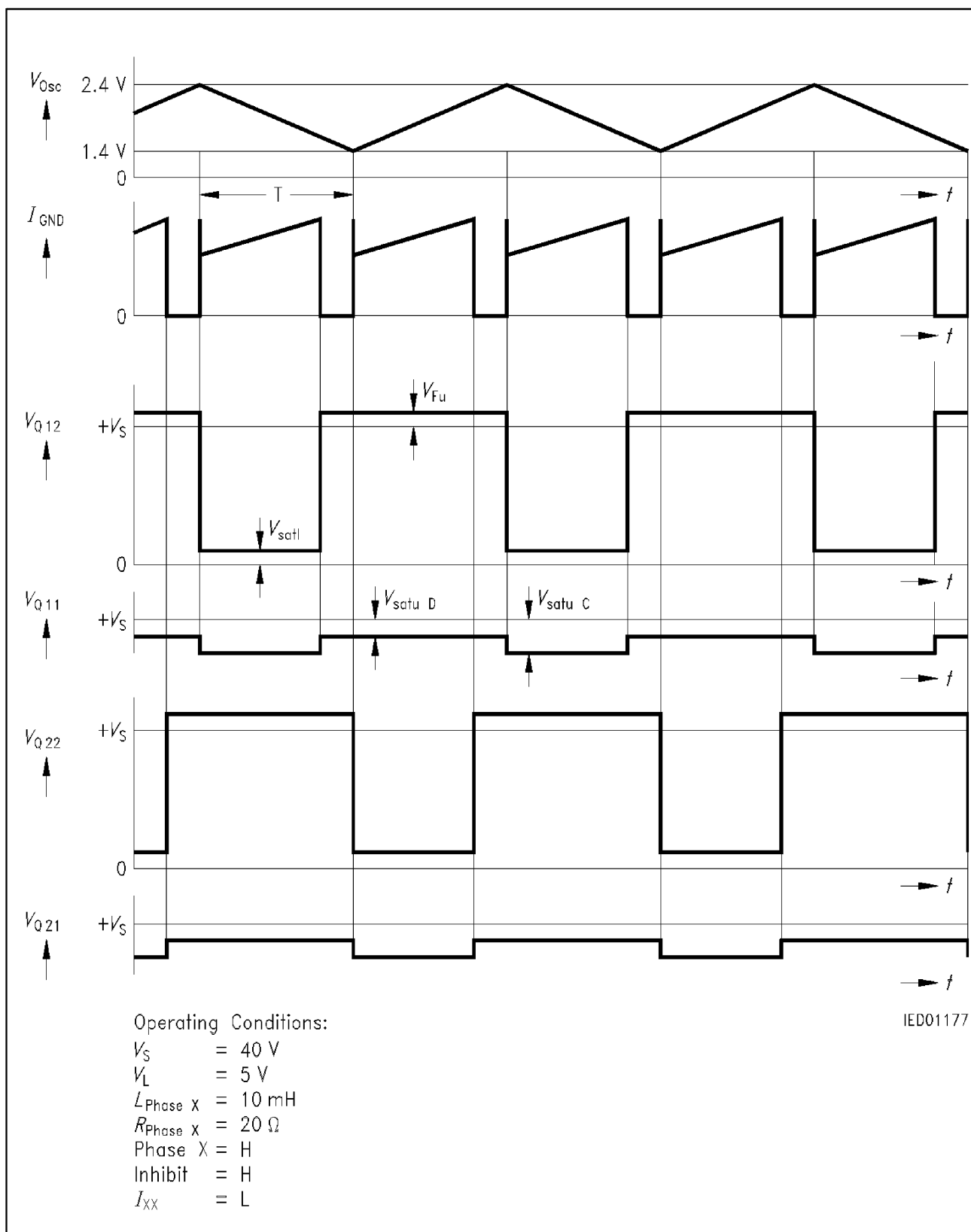


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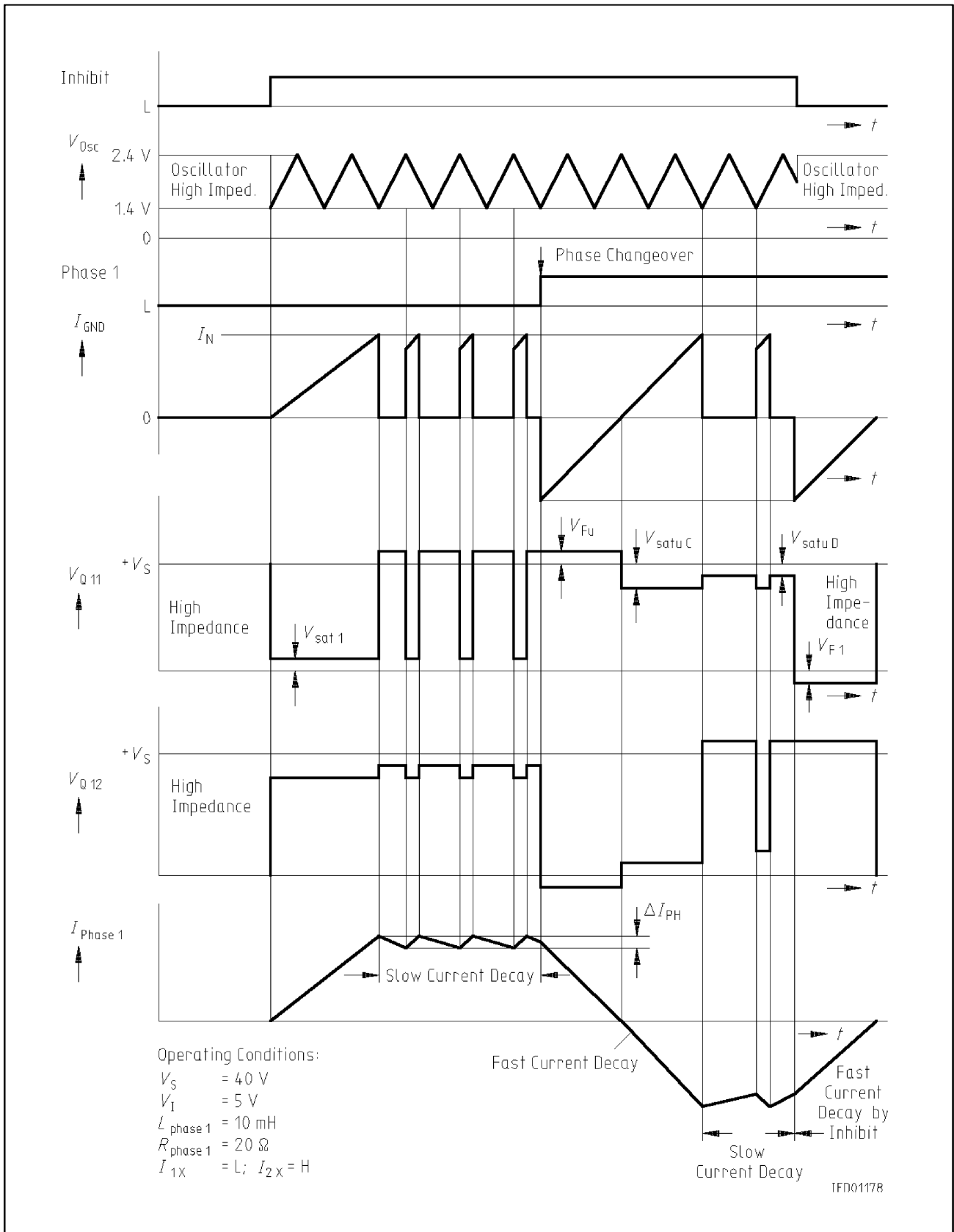
Quarter-Step Operation



Mini-Step Operation



Current Control



Phase Reversal and Inhibit

Calculation of Power Dissipation

The total power dissipation P_{tot} is made up of

- saturation losses P_{sat}** (transistor saturation voltage and diode forward voltages),
- quiescent losses P_q** (quiescent current times supply voltage) and
- switching losses P_s** (turn-ON / turn-OFF operations).

The following equations give the power dissipation for chopper operation without phase reversal. This is the worst case, because full current flows for the entire time and switching losses occur in addition.

$$P_{tot} = 2 \times P_{sat} + P_q + 2 \times P_s$$

where
$$P_{sat} \cong I_N \{ V_{sat1} \times d + V_{Fu} (1 - d) + V_{satuC} \times d + V_{satuD} (1 - d) \}$$

$$P_q = I_q \times V_S + I_L \times V_L$$

$$P_s \cong \frac{V_S}{T} \left\{ \frac{i_D \times t_{DON}}{2} + \frac{i_D + i_R \times t_{ON}}{4} + \frac{I_N}{2} t_{DOFF} + t_{OFF} \right\}$$

I_N = nominal current (mean value)

I_q = quiescent current

i_D = reverse current during turn-on delay

i_R = peak reverse current

t_p = conducting time of chopper transistor

t_{ON} = turn-ON time

t_{OFF} = turn-OFF time

t_{DON} = turn-ON delay

t_{DOFF} = turn-OFFdelay

T = cycle duration

d = duty cycle t_p/T

V_{sat1} = saturation voltage of sink transistor (T3, T4)

V_{satuC} = saturation voltage of source transistor (T1, T2) during charge cycle

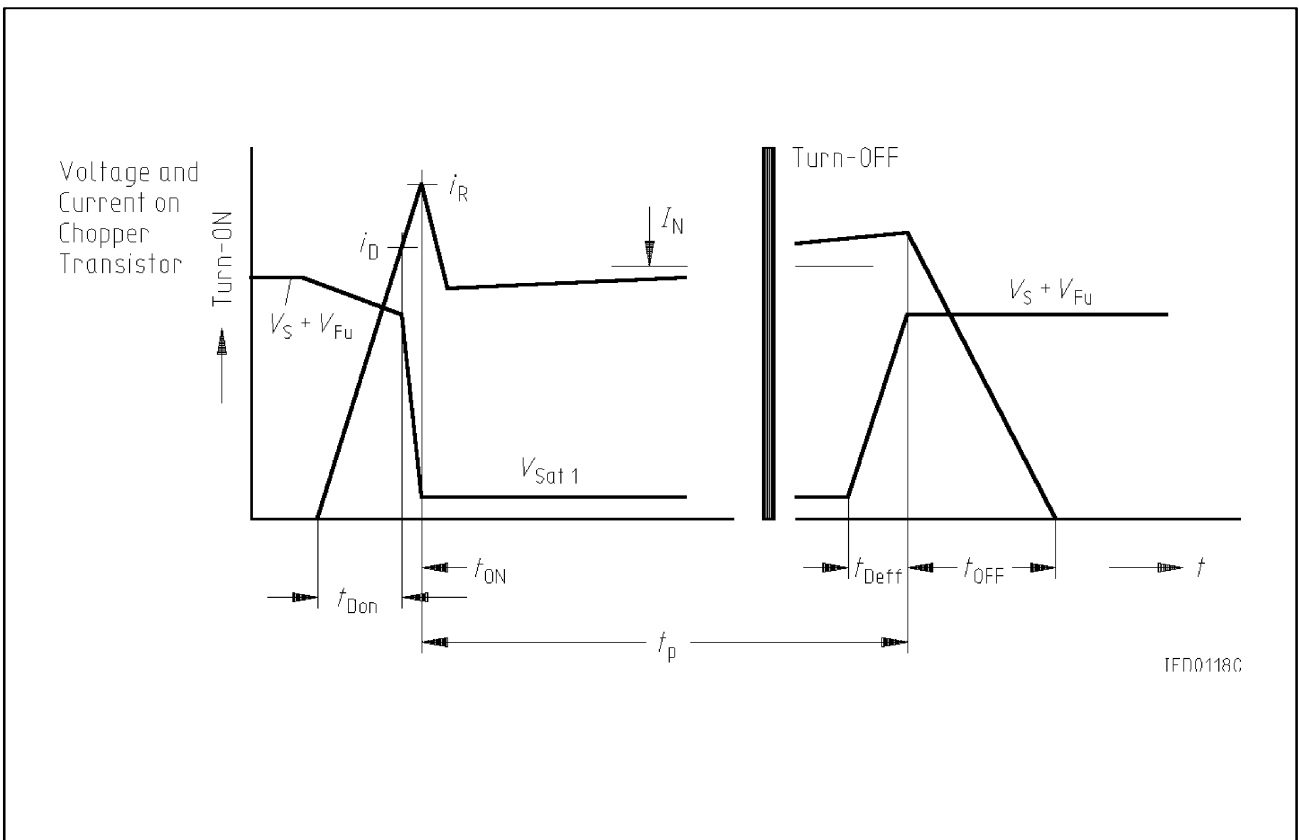
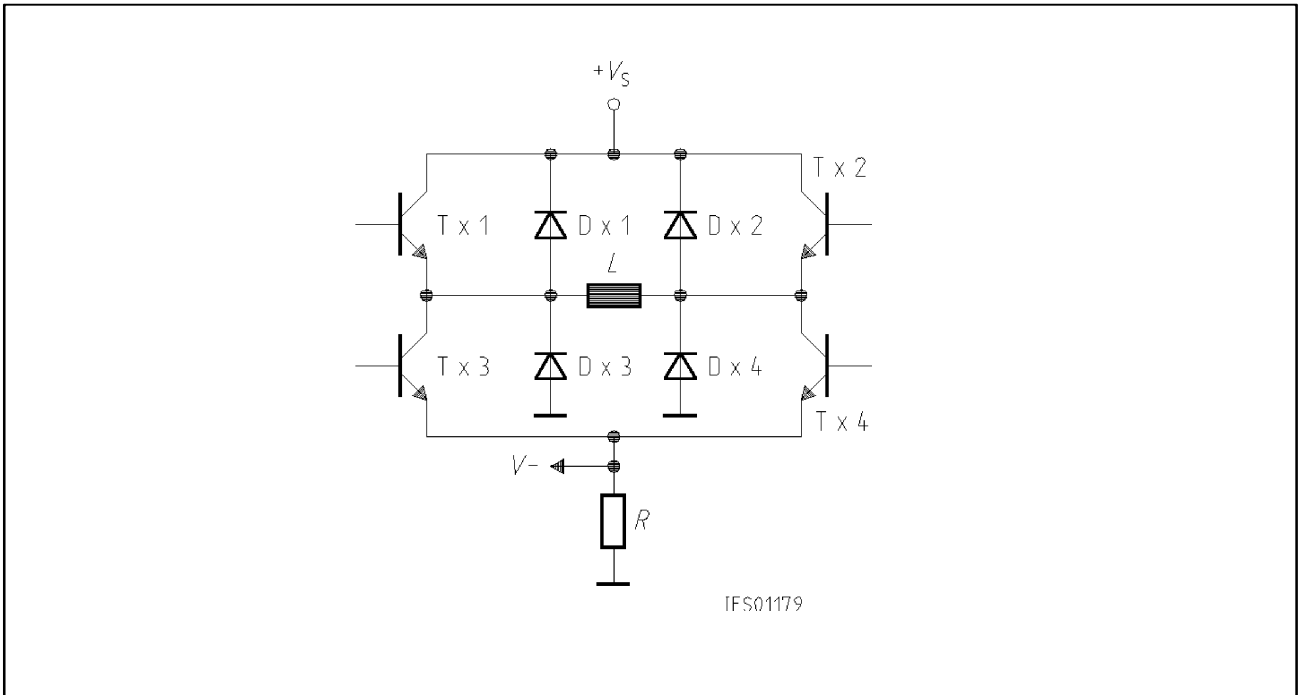
V_{satuD} = saturation voltage of source transistor (T1, T2) during discharge cycle

V_{Fu} = forward voltage of free-wheeling diode (D1, D2)

V_S = supply voltage

V_L = logic supply voltage

I_L = current from logic supply



Application Hints

The TCA 3727 is intended to drive both phases of a stepper motor. Special care has been taken to provide high efficiency, robustness and to minimize external components.

Power Supply

The TCA 3727 will work with supply voltages ranging from 5 V to 50 V at pin V_s . As the circuit operates with chopper regulation of the current, interference generation problems can arise in some applications. Therefore the power supply should be decoupled by a 0.22 μ F ceramic capacitor located near the package. Unstabilized supplies may even afford higher capacities.

Current Sensing

The current in the windings of the stepper motor is sensed by the voltage drop across R_1 and R_2 . Depending on the selected current internal comparators will turn off the sink transistor as soon as the voltage drop reaches certain thresholds (typical 0 V, 0.25 V, 0.5 V and 0.75 V); ($R_1, R_2 = 1 \Omega$). These thresholds are neither affected by variations of V_L nor by variations of V_s .

Due to chopper control fast current rises (up to 10A/ μ s) will occur at the sensing resistors R_1 and R_2 . To prevent malfunction of the current sensing mechanism R_1 and R_2 should be pure ohmic. The resistors should be wired to GND as directly as possible. Capacitive loads such as long cables (with high wire to wire capacity) to the motor should be avoided for the same reason.

Synchronizing Several Choppers

In some applications synchronizing chopping of several stepper motor drivers may be desirable to reduce acoustic interference. This can be done by forcing the oscillator of the TCA 3727 by a pulse generator overdriving the oscillator loading currents (approximately $\geq \pm 100 \mu$ A). In these applications low level should be between 0 V and 1 V while high level should be between 2.6 V and V_L .

Optimizing Noise Immunity

Unused inputs should always be wired to proper voltage levels in order to obtain highest possible noise immunity.

To prevent crossconduction of the output stages the TCA 3727 uses a special break before make timing of the power transistors. This timing circuit can be triggered by short glitches (some hundred nanoseconds) at the Phase inputs causing the output stage to become high resistive during some microseconds. This will lead to a fast current decay during that time. To achieve maximum current accuracy such glitches at the Phase inputs should be avoided by proper control signals.

Thermal Shut Down

To protect the circuit against thermal destruction, thermal shut down has been implemented. To provide a warning in critical applications, the current of the sensing element is wired to input Inhibit. Before thermal shut down occurs Inhibit will start to pull down by some hundred microamperes. This current can be sensed to build a temperature prealarm.