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# High Voltage Half-Bridge Gate Driver with Adaptive Delay

Check for Samples: SM74104

# **FEATURES**

- **Renewable Energy Grade**
- Drives both a High Side and Low Side N-Channel MOSFET
- Adaptive Rising and Falling Edges with • **Programmable Additional Delay**
- Single Input Control
- Bootstrap Supply Voltage Range up to 118V • DC
- Fast Turn-Off Propagation Delay (25 ns Typical)
- Drives 1000 pF Loads with 15 ns Rise and Fall Times
- Supply Rail Under-Voltage Lockout

# TYPICAL APPLICATIONS

- **Current Fed Push-Pull Power Converters**
- **High Voltage Buck Regulators**
- **Active Clamp Forward Power Converters**
- Half and Full Bridge Converters

### PACKAGE

- WSON-10 (4 mm x 4 mm) ٠
- SOIC-8

# DESCRIPTION

The SM74104 High Voltage Gate Driver is designed to drive both the high side and the low side N-Channel MOSFETs in a synchronous buck configuration. The floating high-side driver is capable of working with supply voltages up to 100V. The high side and low side gate drivers are controlled from a single input. Each change in state is controlled in an adaptive manner to prevent shoot-through issues. In addition to the adaptive transition timing, an additional delay time can be added, proportional to an external setting resistor. An integrated high voltage diode is provided to charge the high side gate drive bootstrap capacitor. A robust level shifter operates at high speed while consuming low power and providing clean level transitions from the control logic to the high side gate driver. Under-voltage lockout is provided on both the low side and the high side power rails. This device is available in the standard SOIC-8 pin and the WSON-10 pin packages.



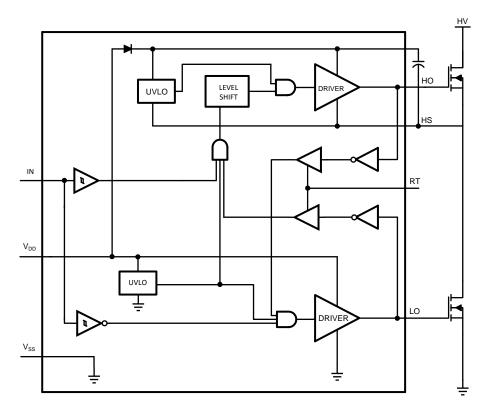
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### SIMPLIFIED BLOCK DIAGRAM



# **Connection Diagrams**





These devices have limited built-in ESD protection. The leads should be shorted together or the device placed in conductive foam during storage or handling to prevent electrostatic damage to the MOS gates.



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### Absolute Maximum Ratings (1)(2)

-0.3V to +18V
-0.3V to +18V
-0.3V to V <sub>DD</sub> + 0.3V
-0.3V to V <sub>DD</sub> + 0.3V
$V_{HS} - 0.3V$ to $V_{HB} + 0.3V$
-1V to +100V
118V
–0.3V to 5V
+150°C
–55°C to +150°C
2 kV

(1) Absolute Maximum Ratings indicate limits beyond which damage to the component may occur. Operating Ratings are conditions under which operation of the device is guaranteed. Operating Ratings do not imply guaranteed performance limits. For guaranteed performance limits and associated test conditions, see the Electrical Characteristics tables.

(2) If Military/Aerospace specified devices are required, please contact the Texas Instruments Sales Office/ Distributors for availability and specifications.N

(3) The human body model is a 100 pF capacitor discharged through a  $1.5k\Omega$  resistor into each pin. 2 kV for all pins except Pin 2, Pin 3 and Pin 4 which are rated at 500V.

### **Recommended Operating Conditions**

V <sub>DD</sub>	+9V to +14V
HS	-1V to 100V
НВ	V <sub>HS</sub> + 8V to V <sub>HS</sub> + 14V
HS Slew Rate	<50V/ns
Junction Temperature	-40°C to +125°C

### **Electrical Characteristics**

Specifications in standard typeface are for  $T_J = +25^{\circ}$ C, and those in **boldface type** apply over the full **operating junction temperature range**. Unless otherwise specified,  $V_{DD} = V_{HB} = 12$ V,  $V_{SS} = V_{HS} = 0$ V, RT = 100k $\Omega$ . No Load on LO or HO.

Symbol	Parameter	Conditions	Min	Тур	Max	Units
SUPPLY CU	RRENTS					
I <sub>DD</sub>	V <sub>DD</sub> Quiescent Current	LI = HI = 0V		0.4	0.6	mA
I <sub>DDO</sub>	V <sub>DD</sub> Operating Current	f = 500 kHz		1.9	3	mA
I <sub>HB</sub>	Total HB Quiescent Current	LI = HI = 0V		0.06	0.2	mA
I <sub>HBO</sub>	Total HB Operating Current	f = 500 kHz		1.3	3	mA
I <sub>HBS</sub>	HB to V <sub>SS</sub> Current, Quiescent	$V_{HS} = V_{HB} = 100V$		0.05	10	μA
I <sub>HBSO</sub>	HB to V <sub>SS</sub> Current, Operating	f = 500 kHz		0.08		mA
INPUT PINS	·					
V <sub>IL</sub>	Low Level Input Voltage Threshold		0.8	1.8		V
V <sub>IH</sub>	High Level Input Voltage Threshold			1.8	2.2	V
R <sub>I</sub>	Input Pulldown Resistance		100	200	500	kΩ
TIME DELAY	CONTROLS					
V <sub>RT</sub>	Nominal Voltage at RT		2.7	3	3.3	V
I <sub>RT</sub>	RT Pin Current Limit	RT = 0V	0.75	1.5	2.25	mA
T <sub>D1</sub>	Delay Timer, RT = 10 kΩ		58	90	130	ns
T <sub>D2</sub>	Delay Timer, RT = 100 kΩ		140	200	270	ns
UNDER VOL	TAGE PROTECTION				•	
V <sub>DDR</sub>	V <sub>DD</sub> Rising Threshold		6.0	6.9	7.4	V
V <sub>DDH</sub>	V <sub>DD</sub> Threshold Hysteresis			0.5		V
V <sub>HBR</sub>	HB Rising Threshold		5.7	6.6	7.1	V

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### **Electrical Characteristics (continued)**

Specifications in standard typeface are for  $T_J = +25^{\circ}$ C, and those in **boldface type** apply over the full **operating junction temperature range**. Unless otherwise specified,  $V_{DD} = V_{HB} = 12V$ ,  $V_{SS} = V_{HS} = 0V$ , RT = 100k $\Omega$ . No Load on LO or HO.

Symbol	Parameter	Conditions	Min	Тур	Max	Units
V <sub>HBH</sub>	HB Threshold Hysteresis			0.4		V
BOOT STRA	AP DIODE					
V <sub>DL</sub>	Low-Current Forward Voltage	I <sub>VDD-HB</sub> = 100 μA		0.60	0.9	V
V <sub>DH</sub>	High-Current Forward Voltage	$I_{VDD-HB} = 100 \text{ mA}$		0.85	1.1	V
R <sub>D</sub>	Dynamic Resistance	$I_{VDD-HB} = 100 \text{ mA}$		0.8	1.5	Ω
LO GATE D	RIVER					
V <sub>OLL</sub>	Low-Level Output Voltage	I <sub>LO</sub> = 100 mA		0.25	0.4	V
V <sub>OHL</sub>	High-Level Output Voltage	$I_{LO} = -100 \text{ mA}$ $V_{OHL} = V_{DD} - V_{LO}$		0.35	0.55	V
I <sub>OHL</sub>	Peak Pullup Current	$V_{LO} = 0V$		1.6		А
I <sub>OLL</sub>	Peak Pulldown Current	$V_{LO} = 12V$		1.8		А
HO GATE D	RIVER					
V <sub>OLH</sub>	Low-Level Output Voltage	I <sub>HO</sub> = 100 mA		0.25	0.4	V
V <sub>OHH</sub>	High-Level Output Voltage	$I_{HO} = -100 \text{ mA},$ $V_{OHH} = V_{HB} - V_{HO}$		0.35	0.55	V
I <sub>ОНН</sub>	Peak Pullup Current	$V_{HO} = 0V$		1.6		А
I <sub>OLH</sub>	Peak Pulldown Current	V <sub>HO</sub> = 12V		1.8		А
THERMAL R	ESISTANCE			·		
$\theta_{JA}$	Junction to Ambient	SOIC-8		170		°C/W
		WSON-10 (1)		40		1

 4 layer board with Cu finished thickness 1.5/1/1/1.5 oz. Maximum die size used. 5x body length of Cu trace on PCB top. 50 x 50mm ground and power planes embedded in PCB. See Application Note AN-1187.

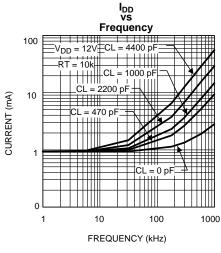
### **Switching Characteristics**

Specifications in standard typeface are for  $T_J = +25^{\circ}C$ , and those in **boldface type** apply over the full **operating junction temperature range**. Unless otherwise specified,  $V_{DD} = V_{HB} = 12V$ ,  $V_{SS} = V_{HS} = 0V$ , No Load on LO or HO.

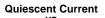
Symbol	Parameter	Conditions	Min	Тур	Max	Units
t <sub>LPHL</sub>	Lower Turn-Off Propagation Delay (IN Rising to LO Falling)			25	56	ns
t <sub>HPHL</sub>	Upper Turn-Off Propagation Delay (IN Falling to HO Falling)			25	56	ns
t <sub>RC</sub> , t <sub>FC</sub>	Either Output Rise/Fall Time	C <sub>L</sub> = 1000 pF		15		ns
t <sub>R</sub> , t <sub>F</sub>	Either Output Rise/Fall Time (3V to 9V)	C <sub>L</sub> = 0.1 μF		0.6		μs
t <sub>BS</sub>	Bootstrap Diode Turn-Off Time	I <sub>F</sub> = 20 mA, I <sub>R</sub> = 200 mA		50		ns

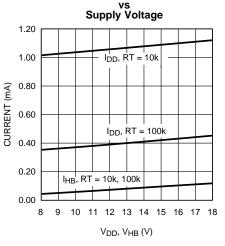


### **Typical Performance Characteristics**

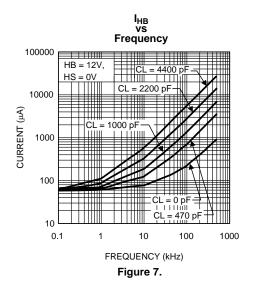


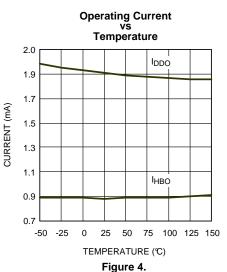
#### Figure 3.



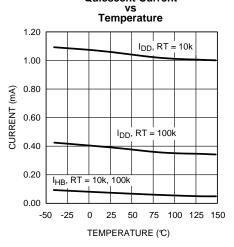






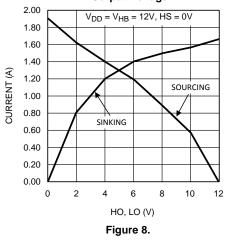


**Quiescent Current** 





HO & LO Peak Output Current vs Output Voltage



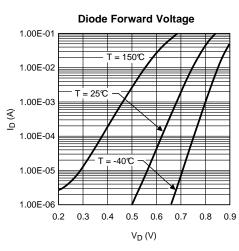
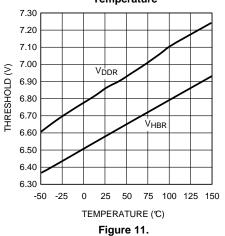
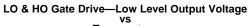
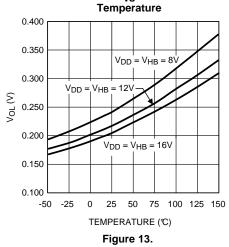


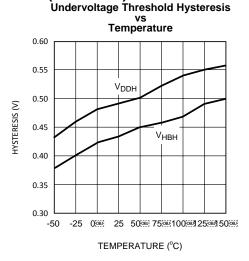
Figure 9.





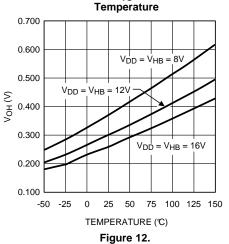




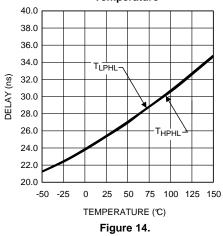


#### Figure 10.

LO & HO Gate Drive—High Level Output Voltage vs







# **Typical Performance Characteristics (continued)**

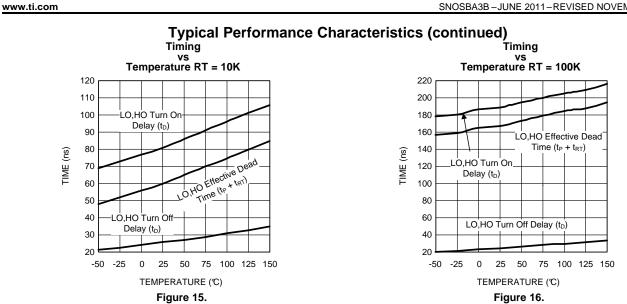
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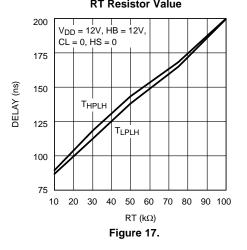
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Turn On Delay vs RT Resistor Value





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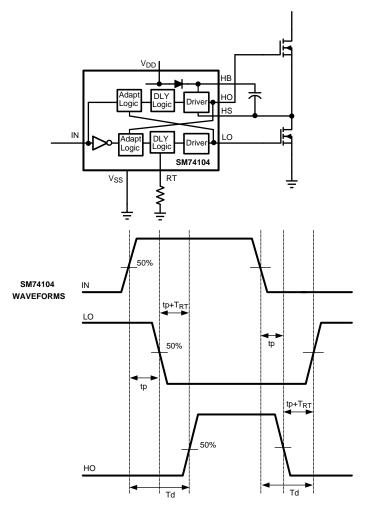


Figure 18. Application Timing Waveforms

# **OPERATIONAL DESCRIPTION**

### ADAPTIVE SHOOT-THROUGH PROTECTION

SM74104 is a high voltage, high speed dual output driver designed to drive top and bottom MOSFET's connected in synchronous buck or half-bridge configuration, from one externally provided PWM signal. SM74104 features adaptive delay to prevent shoot-through current through top and bottom MOSFETs during switching transitions. Referring to the timing diagram Figure 18, the rising edge of the PWM input (IN) turns off the bottom MOSFET (LO) after a short propagation delay (t<sub>P</sub>). An adaptive circuit in the SM74104 monitors the bottom gate voltage (LO) and triggers a programmable delay generator when the LO pin falls below an internally set threshold ( $\approx$  Vdd/2). The gate drive of the upper MOSFET (HO) is disabled until the deadtime expires. The upper gate is enabled after the TIMER delay (t<sub>P</sub>+T<sub>RT</sub>), and the upper MOSFET turns-on. The additional delay of the timer prevents lower and upper MOSFETs from conducting simultaneously, thereby preventing shoot-through.

A falling transition on the PWM signal (IN) initiates the turn-off of the upper MOSFET and turn-on of the lower MOSFET. A short propagation delay (t<sub>P</sub>) is encountered before the upper gate voltage begins to fall. Again, the adaptive shoot-through circuitry and the programmable deadtime TIMER delays the lower gate turn-on time. The upper MOSFET gate voltage is monitored and the deadtime delay generator is triggered when the upper MOSFET gate voltage with respect to ground drops below an internally set threshold ( $\approx$  Vdd/2). The lower gate drive is momentarily disabled by the timer and turns on the lower MOSFET after the deadtime delay expires (t<sub>P</sub>+T<sub>RT</sub>).



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The RT pin is biased at 3V and current limited to 1mA. It is designed to accommodate a resistor between 5K and 100K, resulting in an effective dead-time proportional to RT and ranging from 90ns to 200ns. RT values below 5K will saturate the timer and are not recommended.

### Startup and UVLO

Both top and bottom drivers include under-voltage lockout (UVLO) protection circuitry which monitors the supply voltage ( $V_{DD}$ ) and bootstrap capacitor voltage ( $V_{HB} - V_{HS}$ ) independently. The UVLO circuit inhibits each driver until sufficient supply voltage is available to turn-on the external MOSFETs, and the built-in hysteresis prevents chattering during supply voltage transitions. When the supply voltage is applied to  $V_{DD}$  pin of SM74104, the top and bottom gates are held low until  $V_{DD}$  exceeds UVLO threshold, typically about 6.9V. Any UVLO condition on the bootstrap capacitor will disable only the high side output (HO).

### LAYOUT CONSIDERATIONS

The optimum performance of high and low side gate drivers cannot be achieved without taking due considerations during circuit board layout. Following points are emphasized.

- 1. A low ESR/ESL capacitor must be connected close to the IC, and between V<sub>DD</sub> and V<sub>SS</sub> pins and between HB and HS pins to support high peak currents being drawn from V<sub>DD</sub> during turn-on of the external MOSFET.
- 2. To prevent large voltage transients at the drain of the top MOSFET, a low ESR electrolytic capacitor must be connected between MOSFET drain and ground (V<sub>SS</sub>).
- 3. In order to avoid large negative transients on the switch node (HS) pin, the parasitic inductances in the source of top MOSFET and in the drain of the bottom MOSFET (synchronous rectifier) must be minimized.
- 4. Grounding considerations:
  - The first priority in designing grounding connections is to confine the high peak currents from charging and discharging the MOSFET gate in a minimal physical area. This will decrease the loop inductance and minimize noise issues on the gate terminal of the MOSFET. The MOSFETs should be placed as close as possible to the gate driver.
  - The second high current path includes the bootstrap capacitor, the bootstrap diode, the local ground referenced bypass capacitor and low side MOSFET body diode. The bootstrap capacitor is recharged on the cycle-by-cycle basis through the bootstrap diode from the ground referenced V<sub>DD</sub> bypass capacitor. The recharging occurs in a short time interval and involves high peak current. Minimizing this loop length and area on the circuit board is important to ensure reliable operation.
- 5. The resistor on the RT pin must be placed very close to the IC and seperated from high current paths to avoid noise coupling to the time delay generator which could disrupt timer operation.

### POWER DISSIPATION CONSIDERATIONS

The total IC power dissipation is the sum of the gate driver losses and the bootstrap diode losses. The gate driver losses are related to the switching frequency (f), output load capacitance on LO and HO ( $C_L$ ), and supply voltage ( $V_{DD}$ ) and can be roughly calculated as:

$$\mathsf{P}_{\mathsf{DGATES}} = 2 \bullet \mathsf{f} \bullet \mathsf{C}_{\mathsf{L}} \bullet \mathsf{V}_{\mathsf{DD}}^2$$

(1)

There are some additional losses in the gate drivers due to the internal CMOS stages used to buffer the LO and HO outputs. The following plot shows the measured gate driver power dissipation versus frequency and load capacitance. At higher frequencies and load capacitance values, the power dissipation is dominated by the power losses driving the output loads and agrees well with the above equation. This plot can be used to approximate the power losses due to the gate drivers.

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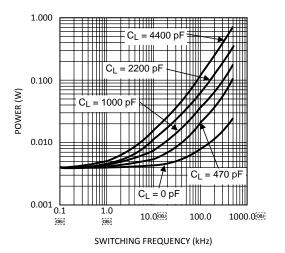


Figure 19. Gate Driver Power Dissipation (LO + HO)  $V_{CC}$  = 12V, Neglecting Diode Losses

The bootstrap diode power loss is the sum of the forward bias power loss that occurs while charging the bootstrap capacitor and the reverse bias power loss that occurs during reverse recovery. Since each of these events happens once per cycle, the diode power loss is proportional to frequency. Larger capacitive loads require more current to recharge the bootstrap capacitor resulting in more losses. Higher input voltages ( $V_{IN}$ ) to the half bridge result in higher reverse recovery losses. The following plot was generated based on calculations and lab measurements of the diode recovery time and current under several operating conditions. This can be useful for approximating the diode power dissipation.

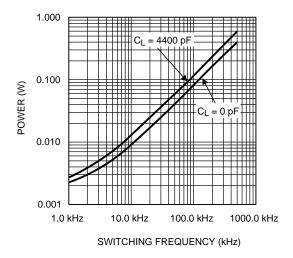


Figure 20. Diode Power Dissipation  $V_{IN} = 80V$ 



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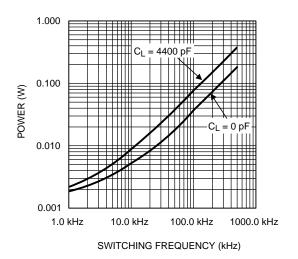


Figure 21. Diode Power Dissipation  $V_{IN} = 40V$ 

The total IC power dissipation can be estimated from the above plots by summing the gate drive losses with the bootstrap diode losses for the intended application. Because the diode losses can be significant, an external diode placed in parallel with the internal bootstrap diode (refer to Figure 22) can be helpful in removing power from the IC. For this to be effective, the external diode must be placed close to the IC to minimize series inductance and have a significantly lower forward voltage drop than the internal diode.

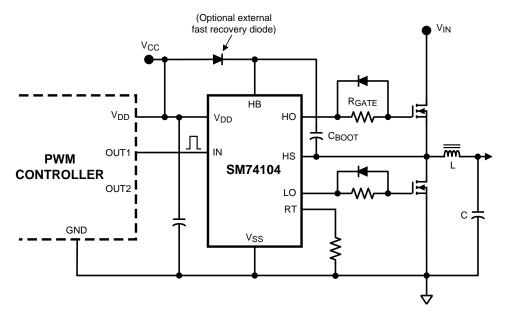


Figure 22. SM74104 Driving MOSFETs Connected in Synchronous Buck Configuration

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